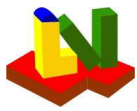


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Layout

Input values:	1.234	or	1.234
Calculated values:	1.234	or	1.234
Critical values:	1.234	or	1.234
Estimated values:	1.234	or	1.234



5 EQU

Form for equations

Tables

with comment every three lines

ASME:2017 Example E4.18.8 and LV-calculation Add 2013

Results are arranged in 3 lines, line1: LV calculation, line 2: ASME,
line 3: difference in %.

:Stationary tubesheet, calculation case 1 -----:-----

	Conversion :	Sig :	SigAll :	Tau :	Tau	Sigto :	Stb :	MaxDiff%
1	145	16416	28493		15196	2563	10662	
2	145	16400	28500		15200	2560	10700	
3	0	0.09598	-0.0254		-0.02539	0.1358	-0.3511	0.3511

:Stationary tubesheet, calculation case 2 -----:-----

	Case 2:	Sig :	SigAll :	Tau :	TauAll :	Sigto :	Stb :	MaxDiff%
4	2	27360	28493		15196	-4522	10662	
5	2	27400	28500		15200	-4520	10700	
6	0	-0.1477	-0.0254		-0.02539	0.05299	-0.3511	0.3511

:Stationary tubesheet, calculation case 3 -----:-----

	Case 3:	Sig :	SigAll :	Tau :	TauAll :	Sigto :	Stb :	MaxDiff%
7	3	10944	28493		15196	-1959	10662	
8	3	10900	28500		15200	-1959	10700	
9	0	0.4019	-0.0254		-0.02539	-4.08e-3	-0.3511	0.3511

:Floating tubesheet, |Sig| for calculation case 1-3 -----:-----

	Case 1 :	Case 2 :	Case 3 :	MaxDiff%
10	9493	15822	6329	
11	9500	15800	6330	
12	-0.07055	0.1403	-0.01791	0

Maximum % difference between LV and ASME for tube and tubesheet stresses:

13	100							
14								
15								

Maximum 2009:

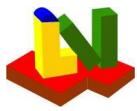
16	0.4582							
----	--------	--	--	--	--	--	--	--

Links

- 1 1 UHXc: psi÷MPa=145: #138*psi÷MPa: #156*psi÷MPa: #140*psi÷MPa: #157*psi÷MPa: #263*psi÷MPa: #269*psi÷MPa
- 2 5 EQU: 145: 16400: 28500: 2210: 15200: 2560: 10700
- 3
- 4 2 UHXc: 2: #138*psi÷MPa: #156*psi÷MPa: #140*psi÷MPa: #157*psi÷MPa: #263*psi÷MPa: #269*psi÷MPa
- 5 5 EQU: 2: 27400: 28500: 3680: 15200: -4520: 10700
- 6
- 7 4 UHXc: 3: #138*psi÷MPa: #156*psi÷MPa: #140*psi÷MPa: #157*psi÷MPa: #263*psi÷MPa: #269*psi÷MPa
- 8 5 EQU: 3: 10900: 28500: 1470: 15200: -1959: 10700
- 9
- 10 3 UHXc: #138(3)*psi÷MPa: #138(9)*psi÷MPa: #138(10)*psi÷MPa
- 11 5 EQU: 9500: 15800: 6330
- 12
- 13 5 EQU: Max(#163;#187;#211;#235)
- 16 '5 EQU: Max(#163;#187;#211;#235)

Additional comments

Units	Value	Unit	Selected Unit
Conversion	#121=	1 MPa	= #123 = 145 psi



Stat

ASME UHX-14 Floating Tubesheets ASME BPVC Edition 2017

Floating tubesheet according to ASME-UHX-14

Type of heat exchanger (a,b,c)	WArt	a	a,b,c
Heat Exchanger With an Immersed Floating Head			
Configuration of the tubesheet (a-f,A-D)	Type	d	a-f,A-D
Stationary tubesheet gasketed with shell and channel			
Type of channel (1=Cylinder, 2=Hemispherical)			1 (1,2)
Shell side internal operation pressure	P _s	250	psi
Tube side internal operation pressure	P _t	150	psi
Shell side internal test pressure	P _{sp}		psi
Tube side internal test pressure	P _{tp}		psi
Load case (1=operation, 2+3=test at 20°C, 4=other)			1
load case: operation			
Calculation case acc. UHX-14.4(a): (1), (2) ... (7)			1 (1-7)
Tube side pressure only (Ps=0) without thermal expansion			

Tubesheet material

Shell material (Type abc)

Tube material

Channel material(Type aefA)

Operation	Tubesheet	Shell	Tubes	Channel
Temperature	°F	°F	°F	°F
Thickness	1.75 in	in	0.083 in	in
Outsidediameter	33.07 in	in	0.75 in	in
Poiss.-rat.	0.31	0.3	0.31	0.3
Allow. c1	0 in	in	0 in	in
Corr.all.c2	0 in	in	0 in	in

Figure

Strength for the selected load case temperature

Strength	psi	psi	psi	psi
Safety				
E-module	2.7e+7 psi	psi	2.7e+7 psi	psi
Therm.dil.	1E-6/°F	1E-6/°F	1E-6/°F	1E-6/°F
Yield str.	psi	psi	20550 psi	psi
Limit	°F	°F	°F	°F
temperature				
All.stress	19000 psi	0 psi	13350 psi	0 psi
Pr.+sec.st	57000 psi	0 psi	psi	psi

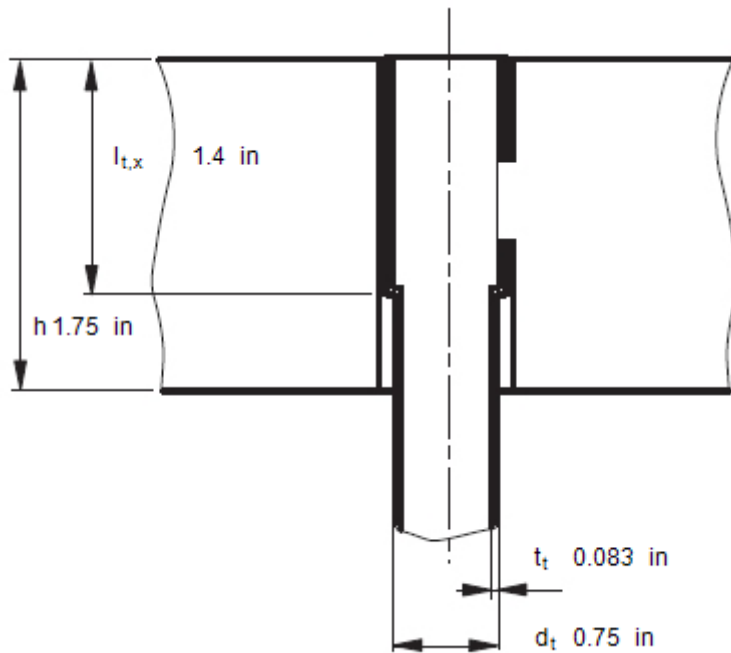
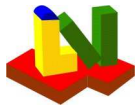
Properties for testing at 20°C

Strength	0 psi	0 psi	0 psi	0 psi
Safety				
Yield str.	psi	psi	psi	psi
Tensile str.	psi	psi	psi	psi

Additional specifications for the geometry and loading

Tubesheet

Tube-tubesheet joint	(1=expanded, 2=welded)	1 (1, 2)
Tube pattern	(1=Triangle, 2=Square)	1 (1, 2)
Number of tubes	N _t	466



Expanded length of tube in tubesheet

Expanded length ratio $l_{t,x}/h$

Radius to outermost tube hole center

Perimeter of the outermost tubes

Total area enclosed by C_p

UHX-11.1(a)

UHX-12.2

UHX-12.2

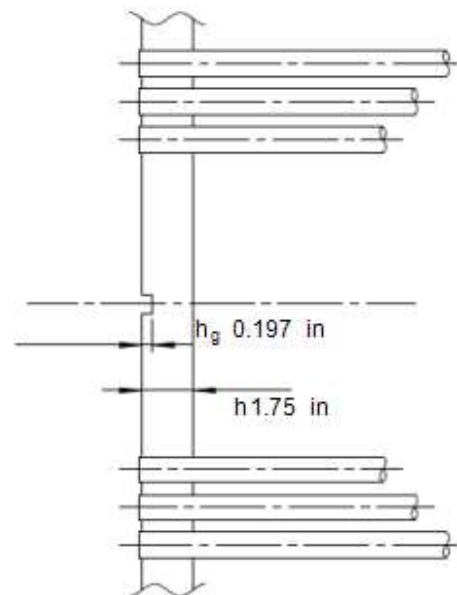
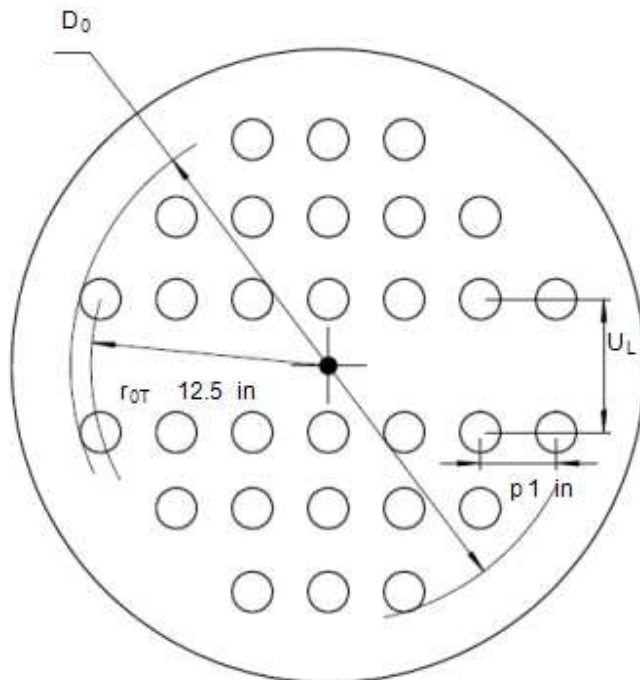
$l_{t,x}$ 1.4 in

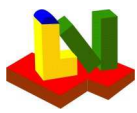
ρ 0.8

r_{0T} 12.5 in

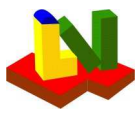
C_p in

A_p in²





Tube pitch (center distance)		p	1	in
Total untubed area $UL1 \cdot LL1 + UL2 \cdot LL2..$	UHX-11.2	A_L	64.4	in ²
Depth of tube side pass partition groove		h_g	0.197	in
Expanded length ratio l_{tx}/h		ρ	0.8	
Tube length between inner tubesheet faces		L	252.5	in
Unsupported tube span for buckling		l		in
Type of tube support (0.6=tubesheet-tubesheet, 0.8=tubesheet - support plate, 1=plate-plate)		k		
Equivalent free buckling length $k \cdot l$		l_t	15.38	in
Flange				
Bolt number		n	-	
Bolt root diameter		d_B		in
Total bolt area		A_b	0	in ²
Bolt material				
Strength operation		K_s		psi
Strength test		K_{sp}		psi
Safety operation		S_s	-	
Safety test		S_{sp}	-	
Stress increase factor (1.5 acc. App.S)		F_s	1.5	-
		Shell		
		Type d,e,f		
			Channel	
			Type B,b,c,d	
Gasket				
Contact outside diameter	G_a	in		in
Contact inside diameter	G_i	in		in
Theoretical seating width	b_0	in		in
Gasket factor (Table 2-5.1)	m			
Gasket seating pressure	Y	psi		0 psi
Diameter of gasket force	G	29.38 in		29.38 in
Poisson's ratio	v	0.3		0.3
		Shell		
			Channel	
Results acc. UHX-9				
Effective seating width	b	in		in
Gasket bolt-up force	W	lbf		lbf
Gasket operating force	W	lbf	211426	lbf
Total required bolt area	A_m	in ²		in ²
Flange thickness	h_r	in		in
Maximum bolt force for all calculation cases			W_{max}	211426 lbf
Bolt root area	0 in ²	:		
Results acc. to UHX-14				
Gasket seating force = $0.5(A_m + A_b) \cdot K_{sp}/S_{sp}$, App.2-5			W	211426 lbf
Channel thickness without allowances			t_c	in
Shell thickness without allowances			t_s	in
Step 1 acc. UHX 14.5				
Basic ligament efficiency for shear		μ	0.25	
Effective ligament efficiency for shear		μ^*	0.3853	
Effective depth of pass partition groove		h_g'	0.197	in
Equivalent radius of outer tube limit circle		a_0	12.87	in
Radial channel dimension		a_c	14.69	in
Radial shell dimension		a_s	14.69	in
Ratio = a_c/a_0		ρ_C	1.141	
Ratio = a_s/a_0		ρ_S	1.141	
Parameter = $1 - N_t \cdot (0.5 \cdot d_a \text{ TUBE}/a_0)^2$		x_s	0.6047	
Parameter = $1 - N_t \cdot (0.5 \cdot d_i \text{ TUBE}/a_0)^2$		x_t	0.7603	
Step 2				



Step 3

Effective modulus of el. tubesheet (Fig.UHX-11.3)

Ratio of elasticity tubesheet

Effective Poisson's ratio tubesheet

Effective pitch

Effective tube hole diameter

Parameter for table UHX-13.1

Z_d 0.03276 Z_v 0.07874 Z_m 0.4213 Z_a 4.21

E^* 1.091e+7 psi

E^*/E 0.4039

v^* 0.3084

p^* 1.068 in

d^* 0.6567 in

X_a 3.61

Z_w 0.07874

Step 4

Diameter ratio = A/D0

F 0.4284 ϕ 0.5605

K 1.284

Q_1 0.07818

UHX-14.5.5 Step 5: Coefficients

ω_C 0 in² ω_S 0 in²

ω_C^* 1.758 in²

ω_S^* 1.758 in²

V_b 0

Results acc. to UHX-14.6 and step 6

T_r = 68 °F T_s^* = 68 °F

P_s^* = 0 psi P_c^* = 0 psi

T_c^* 68 °F

P_e -150 psi

UHX-14.5.7 Step 7

Q_2 -213.4 lbf Q_3 0.09534

Strength condition for the tubesheet bending stress, case

σ = 16420 psi $< 1.5 \cdot \sigma_B$ = 28500 psi

$< S_{PS}$ = 57000 psi

F_m 0.1023

1 :

case 1-3

case 4-7

Step 8

Strength condition for the tubesheet shear stress:

τ = 0 psi $< 0.8 \cdot \sigma_B$ = 15200 psi

Strength condition of step 7-8 are satisfied

Step 9, as examples UHX-20.3:2009 (old N)

F_q 3.421 F_s 1.54

Strength condition for the tube stress with cacluation case

S_{T0} = 2564 psi $\leq \sigma_T$ = 13350 psi

S_{T0} $\leq 2 \cdot \sigma_T$ = 26700 psi

$|S_{T0}|$ $\leq S_{tb}$ = 10665 psi

r_t 0.2376 in F_t 64.72

1 :

for calculation case 1-3

for calculation case 4-7

(for $S_{T0} < 0$, Buckling)

C_t 161

Strength acc. UHX-14.5.9 satisfied

Step 10: Stress σ_S in the shell and σ_C in the channel

$$\begin{aligned} \sigma_S &= |\sigma_{Sm}| + |\sigma_{Sb}| = 0 \text{ psi} < 1.5 \cdot \sigma_{allS}, S_{PSs} \text{ or } S_{PSs1} \text{ psi} \\ \sigma_S &= 0 \text{ psi} < 0 \text{ psi} \\ \sigma_C &= |\sigma_{Cm}| + |\sigma_{Cb}| = 0 \text{ psi} < 1.5 \cdot \sigma_{allC} \text{ or } S_{PSc} \text{ psi} \\ \sigma_C &= 0 \text{ psi} < 0 \text{ psi} \end{aligned}$$

Condition UHX-14.5.10 not required for configurations dBCD

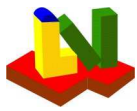
Geometric conditions:

valid

Strength condition for linked modules (Connection activated:

Yes):

Strength conditions are valid for all calculation cases



Stat-2

ASME UHX-14 Floating Tubesheets ASME BPVC Edition 2017

Floating tubesheet according to ASME-UHX-14

Type of heat exchanger (a,b,c)	WArt	a	a,b,c
Heat Exchanger With an Immersed Floating Head			
Configuration of the tubesheet (a-f,A-D)	Type	d	a-f,A-D
Stationary tubesheet gasketed with shell and channel			
Type of channel (1=Cylinder, 2=Hemispherical)			1 (1,2)
Shell side internal operation pressure	P_s	250	psi
Tube side internal operation pressure	P_t	150	psi
Shell side internal test pressure	P_{sp}		psi
Tube side internal test pressure	P_{tp}		psi
Load case (1=operation, 2+3=test at 20°C, 4=other)			1
load case: operation			
Calculation case acc. UHX-14.4(a): (1), (2) ... (7)			2 (1-7)
Shell side pressure only ($P_t=0$) without thermal expansion			

Tubesheet material

Shell material (Type abc)

Tube material

Channel material(Type aefA)

Operation	Tubesheet	Shell	Tubes	Channel
Temperature	°F	°F	°F	°F
Thickness	1.75 in	in	0.083 in	in
Outsidediameter	33.07 in	in	0.75 in	in
Poiss.-rat.	0.31	0.3	0.31	0.3
Allow. c1	0 in	in	0 in	in
Corr.all.c2	0 in	in	0 in	in

Figure

Strength for the selected load case temperature

Strength	psi	psi	psi	psi
Safety				
E-module	2.7e+7 psi	psi	2.7e+7 psi	psi
Therm.dil.	1E-6/°F	1E-6/°F	1E-6/°F	1E-6/°F
Yield str.	psi	psi	20550 psi	psi
Limit	°F	°F	°F	°F
temperature				
All.stress	19000 psi	0 psi	13350 psi	0 psi
Pr.+sec.st	57000 psi	0 psi	psi	psi

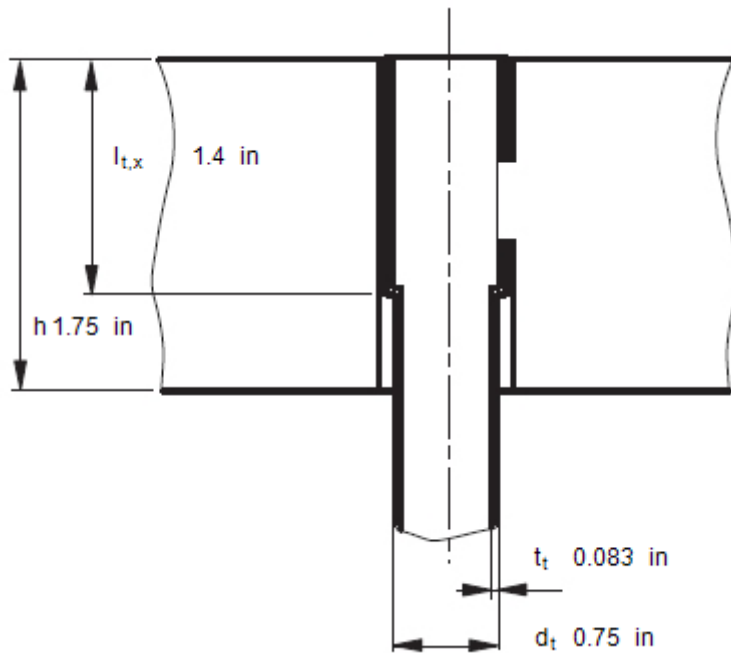
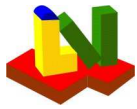
Properties for testing at 20°C

Strength	0 psi	0 psi	0 psi	0 psi
Safety				
Yield str.	psi	psi	psi	psi
Tensile str.	psi	psi	psi	psi

Additional specifications for the geometry and loading

Tubesheet

Tube-tubesheet joint	(1=expanded, 2=welded)	1 (1, 2)
Tube pattern	(1=Triangle, 2=Square)	1 (1, 2)
Number of tubes	N_t	466



Expanded length of tube in tubesheet

Expanded length ratio $l_{t,x}/h$

Radius to outermost tube hole center

Perimeter of the outermost tubes

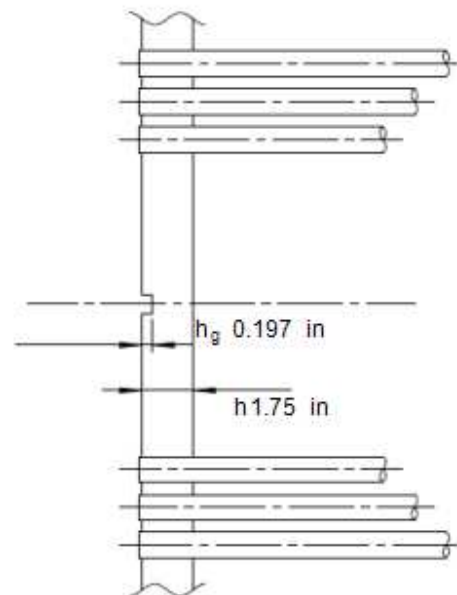
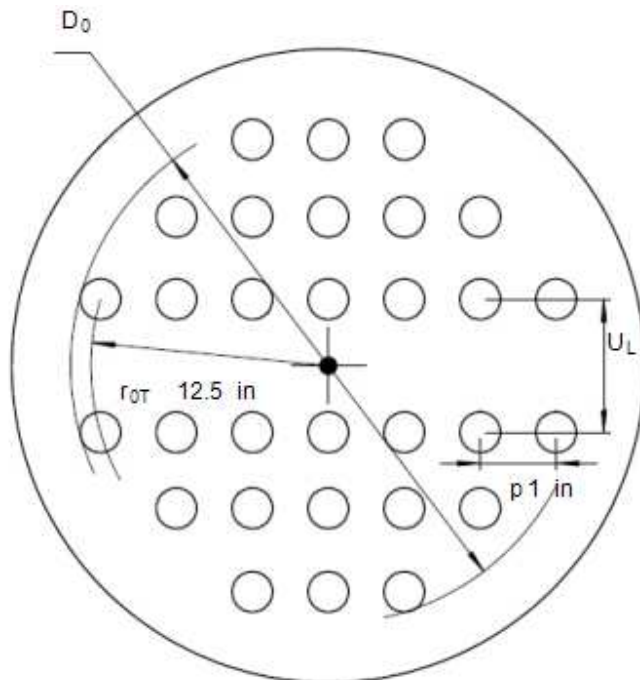
Total area enclosed by C_p

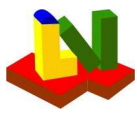
UHX-11.1(a)

UHX-12.2

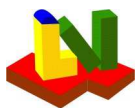
UHX-12.2

$l_{t,x}$	1.4 in
ρ	0.8
r_{0T}	12.5 in
C_p	in
A_p	in ²





Tube pitch (center distance)		p	1	in
Total untubed area $UL1 \cdot LL1 + UL2 \cdot LL2..$	UHX-11.2	A_L	64.4	in ²
Depth of tube side pass partition groove		h_g	0.197	in
Expanded length ratio l_{tx}/h		ρ	0.8	
Tube length between inner tubesheet faces		L	252.5	in
Unsupported tube span for buckling		l		in
Type of tube support (0.6=tubesheet-tubesheet, 0.8=tubesheet - support plate, 1=plate-plate)		k		
Equivalent free buckling length $k \cdot l$		l_t	15.38	in
Flange				
Bolt number		n	-	
Bolt root diameter		d_B		in
Total bolt area		A_b	0	in ²
Bolt material				
Strength operation		K_s		psi
Strength test		K_{sp}		psi
Safety operation		S_s	-	
Safety test		S_{sp}	-	
Stress increase factor (1.5 acc. App.S)		F_s	1.5	-
		Shell	Channel	
		Type d,e,f	Type B,b,c,d	
Gasket				
Contact outside diameter	G_a	in		in
Contact inside diameter	G_i	in		in
Theoretical seating width	b_0	in		in
Gasket factor (Table 2-5.1)	m			
Gasket seating pressure	Y	psi	0	psi
Diameter of gasket force	G	29.38 in	29.38	in
Poisson's ratio	v	0.3	0.3	
Results acc. UHX-9		Shell	Channel	
Effective seating width	b	in		in
Gasket bolt-up force	W	lbf		lbf
Gasket operating force	W	lbf	211426	lbf
Total required bolt area	A_m	in ²		in ²
Flange thickness	h_r	in		in
Maximum bolt force for all calculation cases			W_{max}	211426 lbf
Bolt root area	0 in ²	:		
Results acc. to UHX-14				
Gasket seating force = $0.5(A_m + A_b) \cdot K_{sp}/S_{sp}$, App.2-5		W	211426	lbf
Channel thickness without allowances		t_c		in
Shell thickness without allowances		t_s		in
Step 1 acc. UHX 14.5				
Basic ligament efficiency for shear		μ	0.25	
Effective ligament efficiency for shear		μ^*	0.3853	
Effective depth of pass partition groove		h_g'	0.197	in
Equivalent radius of outer tube limit circle		a_0	12.87	in
Radial channel dimension		a_c	14.69	in
Radial shell dimension		a_s	14.69	in
Ratio = a_c/a_0		ρ_C	1.141	
Ratio = a_s/a_0		ρ_S	1.141	
Parameter = $1 - N_t \cdot (0.5 \cdot d_a \text{ TUBE}/a_0)^2$		x_s	0.6047	
Parameter = $1 - N_t \cdot (0.5 \cdot d_i \text{ TUBE}/a_0)^2$		x_t	0.7603	
Step 2				



Step 3

Effective modulus of el. tubesheet (Fig.UHX-11.3)

Ratio of elasticity tubesheet

Effective Poisson's ratio tubesheet

Effective pitch

Effective tube hole diameter

Parameter for table UHX-13.1

Z_d 0.03276 Z_v 0.07874 Z_m 0.4213 Z_a 4.21

E^* 1.091e+7 psi

E^*/E 0.4039

ν^* 0.3084

p^* 1.068 in

d^* 0.6567 in

X_a 3.61

Z_w 0.07874

Step 4

Diameter ratio = A/D0

F 0.4284 Φ 0.5605

K 1.284

Q_1 0.07818

UHX-14.5.5 Step 5: Coefficients

ω_C 0 in² ω_S 0 in²

ω_C^* 1.758 in²

ω_S^* 1.758 in²

γ_b 0

Results acc. to UHX-14.6 and step 6

T_r = 68 °F T_s^* = 68 °F

P_s^* = 0 psi P_c^* = 0 psi

T_c^* 68 °F

P_e 250 psi

UHX-14.5.7 Step 7

Q_2 355.6 lbf Q_3 0.09534

Strength condition for the tubesheet bending stress, case

σ = 27367 psi $< 1.5 \cdot \sigma_B$ = 28500 psi

$< S_{PS}$ = 57000 psi

F_m 0.1023

2 :

case 1-3

case 4-7

Step 8

Strength condition for the tubesheet shear stress:

τ = 0 psi $< 0.8 \cdot \sigma_B$ = 15200 psi

Strength condition of step 7-8 are satisfied

Step 9, as examples UHX-20.3:2009 (old N)

F_q 3.421 F_s 1.54

Strength condition for the tube stress with cacluation case

S_{T0} = -4524 psi $\leq \sigma_T$ = 13350 psi

S_{T0} $\leq 2 \cdot \sigma_T$ = 26700 psi

$|S_{T0}|$ $\leq S_{tb}$ = 10665 psi

r_t 0.2376 in F_t 64.72

2 :

for calculation case 1-3

for calculation case 4-7

(for $S_{T0} < 0$, Buckling)

C_t 161

Buckling stability acc. UHX-14.5.9 satisfied

Step 10: Stress σ_S in the shell and σ_C in the channel

$$\begin{aligned} \sigma_S &= |\sigma_{Sm}| + |\sigma_{Sb}| = 0 \text{ psi} < 1.5 \cdot \sigma_{allS}, S_{PSs} \text{ or } S_{PSs1} \text{ psi} \\ \sigma_S &= 0 \text{ psi} < 0 \text{ psi} \\ \sigma_C &= |\sigma_{Cm}| + |\sigma_{Cb}| = 0 \text{ psi} < 1.5 \cdot \sigma_{allC} \text{ or } S_{PSc} \text{ psi} \\ \sigma_C &= 0 \text{ psi} < 0 \text{ psi} \end{aligned}$$

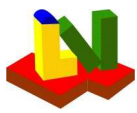
Condition UHX-14.5.10 not required for configurations dBCD

Geometric conditions:

valid

Strength condition for linked modules (Connection activated:

No):



Stat-3

ASME UHX-14 Floating Tubesheets ASME BPVC Edition 2017

Floating tubesheet according to ASME-UHX-14

Type of heat exchanger (a,b,c)	WArt	a	a,b,c
Heat Exchanger With an Immersed Floating Head			
Configuration of the tubesheet (a-f,A-D)	Type	d	a-f,A-D
Stationary tubesheet gasketed with shell and channel			
Type of channel (1=Cylinder, 2=Hemispherical)			1 (1,2)
Shell side internal operation pressure	P_s	250	psi
Tube side internal operation pressure	P_t	150	psi
Shell side internal test pressure	P_{sp}		psi
Tube side internal test pressure	P_{tp}		psi
Load case (1=operation, 2+3=test at 20°C, 4=other)			1
load case: operation			
Calculation case acc. UHX-14.4(a): (1), (2) ... (7)			3 (1-7)
Tube and shell side pressure acting without thermal expansion			

Tubesheet material

Shell material (Type abc)

Tube material

Channel material(Type aefA)

Operation	Tubesheet	Shell	Tubes	Channel
Temperature	°F	°F	°F	°F
Thickness	1.75 in	in	0.083 in	in
Outsidediameter	33.07 in	in	0.75 in	in
Poiss.-rat.	0.31	0.3	0.31	0.3
Allow. c1	0 in	in	0 in	in
Corr.all.c2	0 in	in	0 in	in

Figure

Strength for the selected load case temperature

Strength	psi	psi	psi	psi
Safety				
E-module	2.7e+7 psi	psi	2.7e+7 psi	psi
Therm.dil.	1E-6/°F	1E-6/°F	1E-6/°F	1E-6/°F
Yield str.	psi	psi	20550 psi	psi
Limit	°F	°F	°F	°F
temperature				
All.stress	19000 psi	0 psi	13350 psi	0 psi
Pr.+sec.st	57000 psi	0 psi	psi	psi

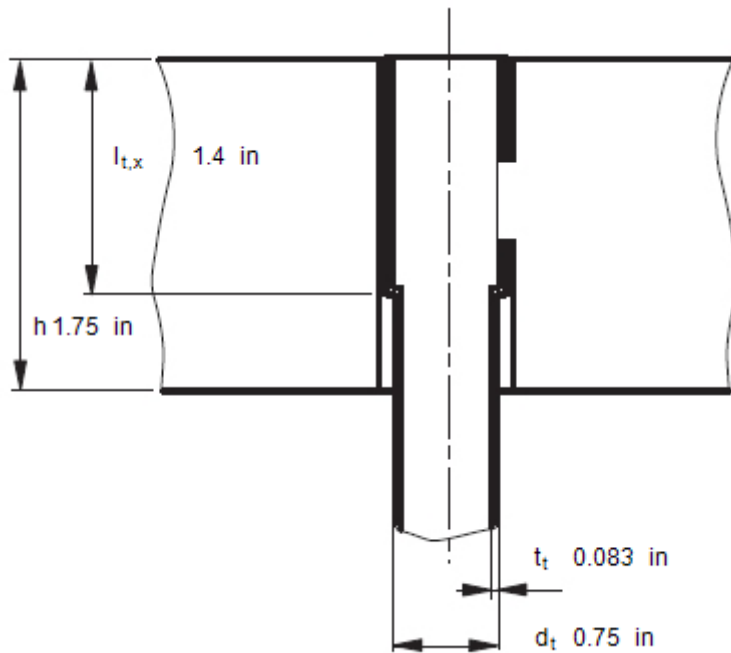
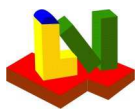
Properties for testing at 20°C

Strength	0 psi	0 psi	0 psi	0 psi
Safety				
Yield str.	psi	psi	psi	psi
Tensile str.	psi	psi	psi	psi

Additional specifications for the geometry and loading

Tubesheet

Tube-tubesheet joint	(1=expanded, 2=welded)	1 (1, 2)
Tube pattern	(1=Triangle, 2=Square)	1 (1, 2)
Number of tubes	N_t	466



Expanded length of tube in tubesheet

Expanded length ratio $l_{t,x}/h$

Radius to outermost tube hole center

Perimeter of the outermost tubes

Total area enclosed by C_p

UHX-11.1(a)

UHX-12.2

UHX-12.2

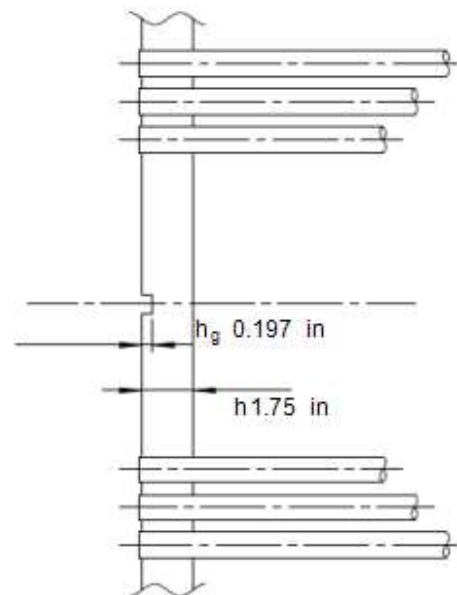
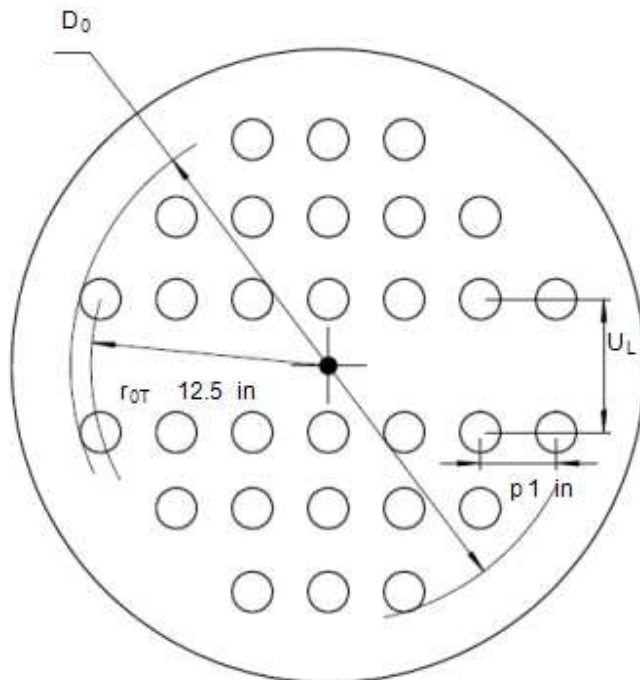
$l_{t,x}$ 1.4 in

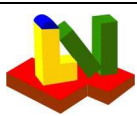
ρ 0.8

r_{0T} 12.5 in

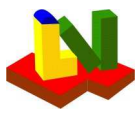
C_p in

A_p in²





Tube pitch (center distance)		p	1	in
Total untubed area UL1·LL1+UL2·LL2..	UHX-11.2	A _L	64.4	in ²
Depth of tube side pass partition groove		h _g	0.197	in
Expanded length ratio l _t /h		ρ	0.8	
Tube length between inner tubesheet faces		L	252.5	in
Unsupported tube span for buckling		l		in
Type of tube support (0.6=tubesheet-tubesheet, 0.8=tubesheet - support plate, 1=plate-plate)		k		
Equivalent free buckling length k · l		l _t	15.38	in
Flange				
Bolt number		n	-	
Bolt root diameter		d _B		in
Total bolt area		A _b	0	in ²
Bolt material				
Strength operation		K _s		psi
Strength test		K _{sp}		psi
Safety operation		S _s	-	
Safety test		S _{sp}	-	
Stress increase factor (1.5 acc. App.S)		F _s	1.5	-
		Shell	Channel	
		Type d,e,f	Type B,b,c,d	
Gasket				
Contact outside diameter	G _a	in		in
Contact inside diameter	G _i	in		in
Theoretical seating width	b ₀	in		in
Gasket factor (Table 2-5.1)	m			
Gasket seating pressure	Y	psi	0	psi
Diameter of gasket force	G	29.38 in	29.38	in
Poisson's ratio	v	0.3	0.3	
Results acc. UHX-9		Shell	Channel	
Effective seating width	b	in		in
Gasket bolt-up force	W	lbf		lbf
Gasket operating force	W	lbf	211426	lbf
Total required bolt area	A _m	in ²		in ²
Flange thickness	h _r	in		in
Maximum bolt force for all calculation cases			W _{max}	211426 lbf
Bolt root area	0 in ²	:		
Results acc. to UHX-14				
Gasket seating force = 0.5(A _m +A _b)·K _{sp} /S _{sp} , App.2-5		W	211426	lbf
Channel thickness without allowances		t _c		in
Shell thickness without allowances		t _s		in
Step 1 acc. UHX 14.5				
Basic ligament efficiency for shear		μ	0.25	
Effective ligament efficiency for shear		μ*	0.3853	
Effective depth of pass partition groove		h _g '	0.197	in
Equivalent radius of outer tube limit circle		a ₀	12.87	in
Radial channel dimension		a _c	14.69	in
Radial shell dimension		a _s	14.69	in
Ratio = a _c /a ₀		ρ _C	1.141	
Ratio = a _s /a ₀		ρ _S	1.141	
Parameter = 1-N _t ·(0.5·d _a TUBE/a ₀) ²		x _s	0.6047	
Parameter = 1-N _t ·(0.5·d _i TUBE/a ₀) ²		x _t	0.7603	
Step 2				



Step 3

Effective modulus of el. tubesheet (Fig.UHX-11.3)

Ratio of elasticity tubesheet

Effective Poisson's ratio tubesheet

Effective pitch

Effective tube hole diameter

Parameter for table UHX-13.1

Z_d 0.03276 Z_v 0.07874 Z_m 0.4213 Z_a 4.21

E^* 1.091e+7 psi

E^*/E 0.4039

ν^* 0.3084

p^* 1.068 in

d^* 0.6567 in

X_a 3.61

Z_w 0.07874

Step 4

Diameter ratio = A/D0

F 0.4284 ϕ 0.5605

K 1.284

Q_1 0.07818

UHX-14.5.5 Step 5: Coefficients

ω_C 0 in² ω_S 0 in² ω_C^* 1.758 in²

ω_S^* 1.758 in²

γ_b 0

Results acc. to UHX-14.6 and step 6

T_r = 68 °F T_s^* = 68 °F

P_s^* = 0 psi P_c^* = 0 psi

T_c^* 68 °F

P_e 100 psi

UHX-14.5.7 Step 7

Q_2 142.2 lbf Q_3 0.09534

Strength condition for the tubesheet bending stress, case

σ = 10947 psi $< 1.5 \cdot \sigma_B$ = 28500 psi

$< S_{PS}$ = 57000 psi

F_m 0.1023

3 :

case 1-3

case 4-7

Step 8

Strength condition for the tubesheet shear stress:

τ = 0 psi $< 0.8 \cdot \sigma_B$ = 15200 psi

Strength condition of step 7-8 are satisfied

Step 9, as examples UHX-20.3:2009 (old N)

F_q 3.421 F_s 1.54

Strength condition for the tube stress with cacluation case

S_{T0} = -1959 psi $\leq \sigma_T$ = 13350 psi

S_{T0} $\leq 2 \cdot \sigma_T$ = 26700 psi

$|S_{T0}|$ $\leq S_{tb}$ = 10665 psi

r_t 0.2376 in F_t 64.72

3 :

for calculation case 1-3

for calculation case 4-7

(for $S_{T0} < 0$, Buckling)

C_t 161

Buckling stability acc. UHX-14.5.9 satisfied

Step 10: Stress σ_S in the shell and σ_C in the channel

$\sigma_S = |\sigma_{Sm}| + |\sigma_{Sb}| = 0$ psi $< 1.5 \cdot \sigma_{allS}, S_{PSs}$ or S_{PSs1} psi

$\sigma_S = 0$ psi $|+| 0$ psi < 0 psi

$\sigma_C = |\sigma_{Cm}| + |\sigma_{Cb}| = 0$ psi $< 1.5 \cdot \sigma_{allC}$ or S_{PSc} psi

$\sigma_C = 0$ psi $|+| 0$ psi < 0 psi

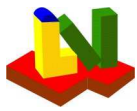
Condition UHX-14.5.10 not required for configurations dBCD

Geometric conditions:

valid

Strength condition for linked modules (Connection activated:

No):



Float

ASME UHX-14 Floating Tubesheets ASME BPVC Edition 2017

Floating tubesheet according to ASME-UHX-14

Type of heat exchanger (a,b,c)	WArt	a	a,b,c
Heat Exchanger With an Immersed Floating Head			
Configuration of the tubesheet (a-f,A-D)	Type	C	a-f,A-D
Floating tubesheet gasketed, without flange extension			
Type of channel (1=Cylinder, 2=Hemispherical)			1 (1,2)
Shell side internal operation pressure	P_s	250	psi
Tube side internal operation pressure	P_t	150	psi
Shell side internal test pressure	P_{sp}		psi
Tube side internal test pressure	P_{tp}		psi
Load case (1=operation, 2+3=test at 20°C, 4=other)			1
load case: operation			
Calculation case acc. UHX-14.4(a): (1), (2) ... (7)			1 (1-7)
Tube side pressure only ($P_s=0$) without thermal expansion			

Tubesheet material

Shell material (Type abc)

Tube material

Channel material(Type aefA)

Operation	Tubesheet	Shell	Tubes	Channel
Temperature	°F	°F	°F	°F
Thickness	1.75 in	in	0.083 in	0.3125 in
Outsidediameter	26.89 in	in	0.75 in	27.03 in
Poiss.-rat.	0.31	0.3	0.31	0.32
Allow. c1	0 in	in	0 in	0 in
Corr.all.c2	0 in	in	0 in	0 in

Figure

Strength for the selected load case temperature

Strength	psi	psi	psi	psi
Safety				
E-module	2.7e+7 psi	psi	2.7e+7 psi	1.48e+7 psi
Therm.dil.	1E-6/°F	1E-6/°F	1E-6/°F	4.8 1E-6/°F
Yield str.	psi	psi	20550 psi	31600 psi
Limit	°F	°F	°F	°F
temperature				
All.stress	19000 psi	0 psi	13350 psi	11300 psi
Pr.+sec.st	57000 psi	0 psi	psi	33900 psi

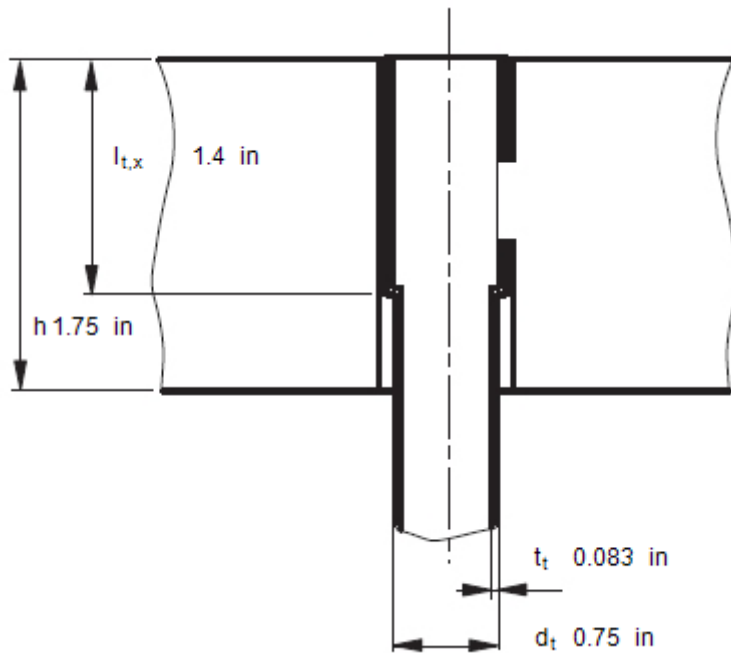
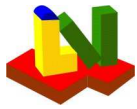
Properties for testing at 20°C

Strength	0 psi	0 psi	0 psi	0 psi
Safety				
Yield str.	psi	psi	psi	psi
Tensile str.	psi	psi	psi	psi

Additional specifications for the geometry and loading

Tubesheet

Tube-tubesheet joint	(1=expanded, 2=welded)	1 (1, 2)
Tube pattern	(1=Triangle, 2=Square)	1 (1, 2)
Number of tubes	N_t	466



Expanded length of tube in tubesheet

Expanded length ratio $l_{t,x}/h$

Radius to outermost tube hole center

Perimeter of the outermost tubes

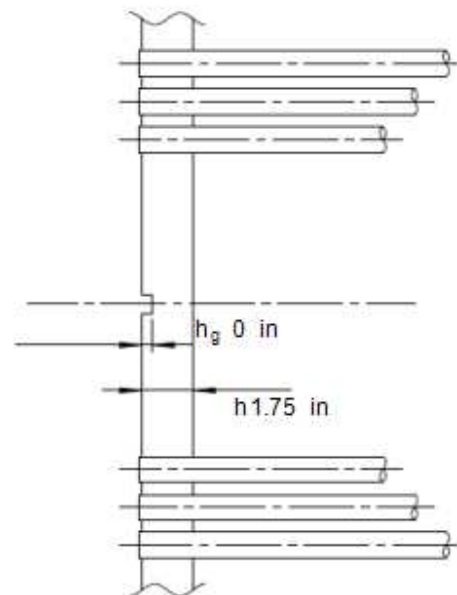
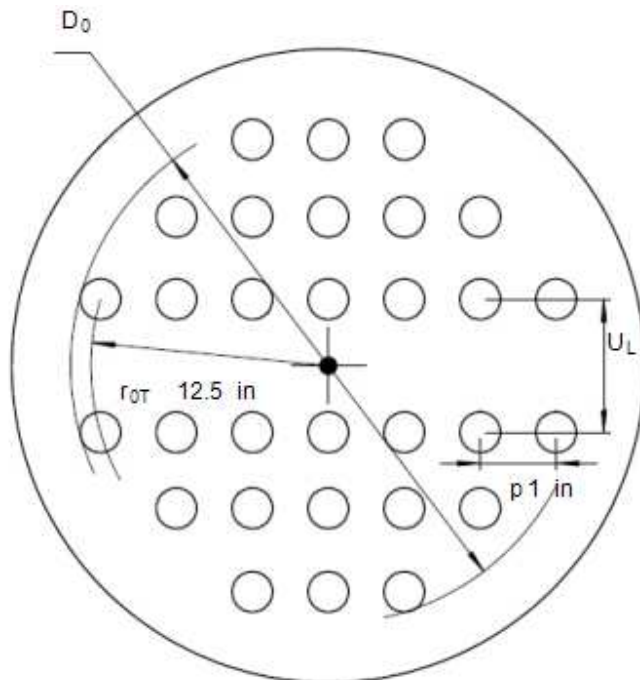
Total area enclosed by C_p

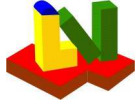
UHX-11.1(a)

UHX-12.2

UHX-12.2

$l_{t,x}$	1.4 in
ρ	0.8
r_{0T}	12.5 in
C_p	in
A_p	in ²





Tube pitch (center distance)
 Total untubed area $UL1 \cdot LL1 + UL2 \cdot LL2..$ UHX-11.2
 Depth of tube side pass partition groove
 Expanded length ratio ltx/h
 Tube length between inner tubesheet faces
 Unsupported tube span for buckling
 Type of tube support (0.6=tubesheet-tubesheet, 0.8=tubesheet - support plate, 1=plate-plate)
 Equivalent free buckling length $k \cdot l$

p 1 in
 A_L 64.4 in²
 h_g 0 in
 ρ 0.8
 L 252.5 in
 l in
 k
 l_t 15.38 in

Results acc. UHX-9

Shell

Channel

Effective seating width b in
 Gasket bolt-up force W 0 lbf
 Gasket operating force W 0 lbf
 Total required bolt area A_m 0 in²
 Flange thickness h_r 0 in

in
 lbf
 26225 lbf
 0 in²
 0 in

Maximum bolt force for all calculation cases
 Bolt root area 0 in² : **sufficient**

W_{max} 0 lbf

Results acc. to UHX-14

Gasket seating force = $0.5(A_m + A_b) \cdot K_{sp}/S_{sp}$, App.2-5
 Channel thickness without allowances
 Shell thickness without allowances

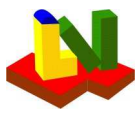
W 26225 lbf
 t_c 0.3125 in
 t_s in

Step 1 acc. UHX 14.5

Basic ligament efficiency for shear
 Effective ligament efficiency for shear
 Effective depth of pass partition groove
 Equivalent radius of outer tube limit circle
 Radial channel dimension
 Radial shell dimension
 Ratio = a_c/a_0
 Ratio = a_s/a_0
 Parameter = $1 - N_t \cdot (0.5 \cdot d_a \text{ TUBE}/a_0)^2$
 Parameter = $1 - N_t \cdot (0.5 \cdot d_i \text{ TUBE}/a_0)^2$

μ 0.25
 μ^* 0.3853
 h_g' 0 in
 a_0 12.87 in
 a_c 13.25 in
 a_s 13.25 in
 ρ_C 1.029
 ρ_S 1.029
 x_s 0.6047
 x_t 0.7603

Step 2



Step 3

Effective modulus of el. tubesheet (Fig.UHX-11.3)

Ratio of elasticity tubesheet

Effective Poisson's ratio tubesheet

Effective pitch

Effective tube hole diameter

Parameter for table UHX-13.1

Z_d **0.03276** Z_v **0.07874** Z_m **0.4213** Z_a **4.21** Z_w **0.07874**

E^* **1.091e+7** psi

E^*/E **0.4039**

ν^* **0.3084**

p^* **1.068** in

d^* **0.6567** in

X_a **3.61**

Step 4

Diameter ratio = A/D0

F **0.07417** ϕ **0.09705** K **1.044**

UHX-14.5.5 Step 5: Coefficients

ω_C **0** in² ω_S **0** in² ω_S^* **0.07057** in² γ_b **0**

Results acc. to UHX-14.6 and step 6

T_r = **68** °F T_s^* = **68** °F T_c^* **68** °F

P_s^* = **0** psi P_c^* = **0** psi P_e **-150** psi

UHX-14.5.7 Step 7

Q_2 **-10.17** lbf Q_3 **0.02131** F_m **0.0751**

Strength condition for the tubesheet bending stress, case

σ = **9496** psi $< 1.5 \cdot \sigma_B$ = **28500** psi case 1-3
 $< S_{PS}$ = **57000** psi case 4-7

Step 8

Strength condition for the tubesheet shear stress:

τ = **0** psi $< 0.8 \cdot \sigma_B$ = **15200** psi

Strength condition of step 7-8 are satisfied

Step 9, as examples UHX-20.3:2009 (old N)

F_q **2.925** F_s **1.787**

Strength condition for the tube stress with cacluation case

S_{T0} = **2087** psi $\leq \sigma_T$ = **13350** psi for calculation case 1-3

S_{T0} $\leq 2 \cdot \sigma_T$ = **26700** psi for calculation case 4-7

$|S_{T0}|$ $\leq S_{tb}$ = **9188** psi (for $S_{T0} < 0$, Buckling)

r_t **0.2376** in F_t **64.72** C_t **161**

Condition UHX-14.5.9 not required for configuration ABCD

Step 10: Stress σ_S in the shell and σ_C in the channel

$\sigma_S = |\sigma_{Sm}| + |\sigma_{Sb}| =$ **0** psi $< 1.5 \cdot \sigma_{allS}, S_{PSs}$ or S_{PSs1} psi
 $\sigma_S =$ **0** psi $|+|$ **0** psi $<$ **0** psi
 $\sigma_C = |\sigma_{Cm}| + |\sigma_{Cb}| =$ **0** psi $< 1.5 \cdot \sigma_{allC}$ or S_{PSc} psi
 $\sigma_C =$ **0** psi $|+|$ **0** psi $<$ **16950** psi

Condition UHX-14.5.10 not required for configurations dBCD

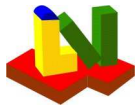
Geometric conditions:

valid

Strength condition for linked modules (Connection activated:

Yes):

Strength conditions are valid for all calculation cases



Float-2

ASME UHX-14 Floating Tubesheets ASME BPVC Edition 2017

Floating tubesheet according to ASME-UHX-14

Type of heat exchanger (a,b,c)	WArt	a	a,b,c
Heat Exchanger With an Immersed Floating Head			
Configuration of the tubesheet (a-f,A-D)	Type	C	a-f,A-D
Floating tubesheet gasketed, without flange extension			
Type of channel (1=Cylinder, 2=Hemispherical)			1 (1,2)
Shell side internal operation pressure	P_s	250	psi
Tube side internal operation pressure	P_t	150	psi
Shell side internal test pressure	P_{sp}		psi
Tube side internal test pressure	P_{tp}		psi
Load case (1=operation, 2+3=test at 20°C, 4=other)			1
load case: operation			
Calculation case acc. UHX-14.4(a): (1), (2) ... (7)			2 (1-7)
Shell side pressure only ($P_t=0$) without thermal expansion			

Tubesheet material

Shell material (Type abc)

Tube material

Channel material(Type aefA)

Operation	Tubesheet	Shell	Tubes	Channel
Temperature	°F	°F	°F	°F
Thickness	1.75 in	in	0.083 in	0.3125 in
Outsidediameter	26.89 in	in	0.75 in	27.03 in
Poiss.-rat.	0.31	0.3	0.31	0.32
Allow. c1	0 in	in	0 in	0 in
Corr.all.c2	0 in	in	0 in	0 in

Figure

Strength for the selected load case temperature

Strength	psi	psi	psi	psi
Safety				
E-module	2.7e+7 psi	psi	2.7e+7 psi	1.48e+7 psi
Therm.dil.	1E-6/°F	1E-6/°F	1E-6/°F	4.8 1E-6/°F
Yield str.	psi	psi	20550 psi	31600 psi
Limit	°F	°F	°F	°F
temperature				
All.stress	19000 psi	0 psi	13350 psi	11300 psi
Pr.+sec.st	57000 psi	0 psi	psi	33900 psi

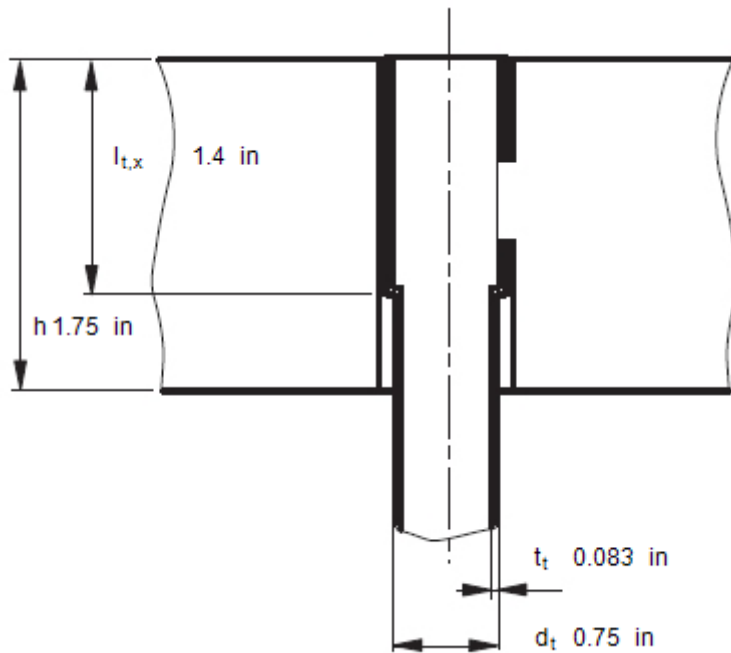
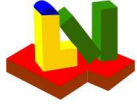
Properties for testing at 20°C

Strength	0 psi	0 psi	0 psi	0 psi
Safety				
Yield str.	psi	psi	psi	psi
Tensile str.	psi	psi	psi	psi

Additional specifications for the geometry and loading

Tubesheet

Tube-tubesheet joint	(1=expanded, 2=welded)	1 (1, 2)
Tube pattern	(1=Triangle, 2=Square)	1 (1, 2)
Number of tubes	N_t	466



Expanded length of tube in tubesheet

Expanded length ratio $l_{t,x}/h$

Radius to outermost tube hole center

Perimeter of the outermost tubes

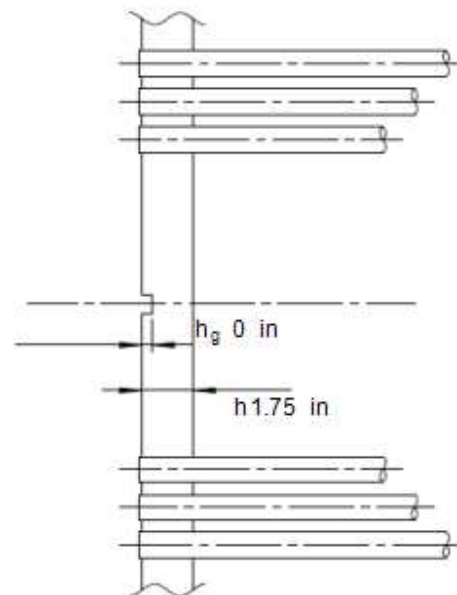
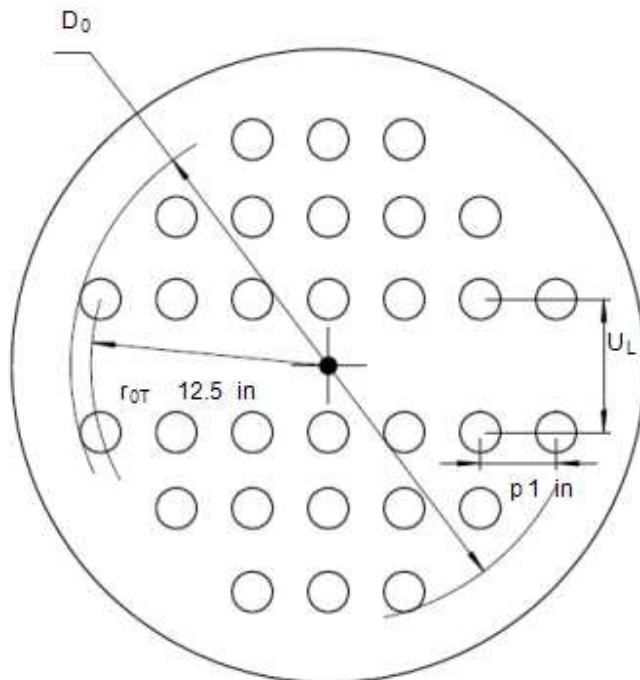
Total area enclosed by C_p

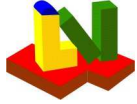
UHX-11.1(a)

UHX-12.2

UHX-12.2

$l_{t,x}$	1.4 in
ρ	0.8
r_{0T}	12.5 in
C_p	in
A_p	in ²





Tube pitch (center distance)
 Total untubed area $UL1 \cdot LL1 + UL2 \cdot LL2..$ UHX-11.2
 Depth of tube side pass partition groove
 Expanded length ratio lt_x/h
 Tube length between inner tubesheet faces
 Unsupported tube span for buckling
 Type of tube support (0.6=tubesheet-tubesheet, 0.8=tubesheet - support plate, 1=plate-plate)
 Equivalent free buckling length $k \cdot l$

p 1 in
 A_L 64.4 in²
 h_g 0 in
 ρ 0.8
 L 252.5 in
 l in
 k
 l_t 15.38 in

Results acc. UHX-9

Shell

Channel

Effective seating width b in
 Gasket bolt-up force W 0 lbf
 Gasket operating force W 0 lbf
 Total required bolt area A_m 0 in²
 Flange thickness h_r 0 in

in
 lbf
 26225 lbf
 0 in²
 0 in

Maximum bolt force for all calculation cases
 Bolt root area 0 in² : **sufficient**

W_{max} 0 lbf

Results acc. to UHX-14

Gasket seating force = $0.5(A_m + A_b) \cdot K_{sp}/S_{sp}$, App.2-5
 Channel thickness without allowances
 Shell thickness without allowances

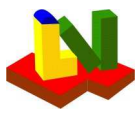
W 26225 lbf
 t_c 0.3125 in
 t_s in

Step 1 acc. UHX 14.5

Basic ligament efficiency for shear
 Effective ligament efficiency for shear
 Effective depth of pass partition groove
 Equivalent radius of outer tube limit circle
 Radial channel dimension
 Radial shell dimension
 Ratio = a_c/a_0
 Ratio = a_s/a_0
 Parameter = $1 - N_t \cdot (0.5 \cdot d_a \text{ TUBE}/a_0)^2$
 Parameter = $1 - N_t \cdot (0.5 \cdot d_i \text{ TUBE}/a_0)^2$

μ 0.25
 μ^* 0.3853
 h_g' 0 in
 a_0 12.87 in
 a_c 13.25 in
 a_s 13.25 in
 ρ_C 1.029
 ρ_S 1.029
 x_s 0.6047
 x_t 0.7603

Step 2



Step 3

Effective modulus of el. tubesheet (Fig.UHX-11.3)

Ratio of elasticity tubesheet

Effective Poisson's ratio tubesheet

Effective pitch

Effective tube hole diameter

Parameter for table UHX-13.1

Z_d 0.03276 Z_v 0.07874 Z_m 0.4213 Z_a 4.21

E^* 1.091e+7 psi

E^*/E 0.4039

ν^* 0.3084

p^* 1.068 in

d^* 0.6567 in

X_a 3.61

Z_w 0.07874

Step 4

Diameter ratio = A/D0

F 0.07417 ϕ 0.09705

K 1.044

Q_1 0.02049

UHX-14.5.5 Step 5: Coefficients

ω_C 0 in² ω_S 0 in² ω_C^* 0.07057 in²

ω_S^* 0.07057 in²

γ_b 0

Results acc. to UHX-14.6 and step 6

T_r = 68 °F T_s^* = 68 °F

P_s^* = 0 psi P_c^* = 0 psi

T_c^* 68 °F

P_e 250 psi

UHX-14.5.7 Step 7

Q_2 16.95 lbf Q_3 0.02131

Strength condition for the tubesheet bending stress, case

σ = 15826 psi $< 1.5 \cdot \sigma_B$ = 28500 psi $< S_{PS}$ = 57000 psi

F_m 0.0751

2 :

case 1-3

case 4-7

Step 8

Strength condition for the tubesheet shear stress:

τ = 0 psi $< 0.8 \cdot \sigma_B$ = 15200 psi

Strength condition of step 7-8 are satisfied

Step 9, as examples UHX-20.3:2009 (old N)

F_q 2.925 F_s 1.787

Strength condition for the tube stress with cacluation case

S_{T0} = -3728 psi $\leq \sigma_T$ = 13350 psi

S_{T0} $\leq 2 \cdot \sigma_T$ = 26700 psi

$|S_{T0}|$ $\leq S_{tb}$ = 9188 psi

r_t 0.2376 in F_t 64.72

2 :

for calculation case 1-3

for calculation case 4-7

(for $S_{T0} < 0$, Buckling)

C_t 161

Condition UHX-14.5.9 not required for configuration ABCD

Step 10: Stress σ_S in the shell and σ_C in the channel

$\sigma_S = |\sigma_{Sm}| + |\sigma_{Sb}| = 0$ psi $< 1.5 \cdot \sigma_{allS}, S_{PSs}$ or S_{PSs1} psi

$\sigma_S = 0$ psi $|+| 0$ psi < 0 psi

$\sigma_C = |\sigma_{Cm}| + |\sigma_{Cb}| = 0$ psi $< 1.5 \cdot \sigma_{allC}$ or S_{PSc} psi

$\sigma_C = 0$ psi $|+| 0$ psi < 16950 psi

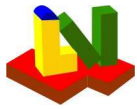
Condition UHX-14.5.10 not required for configurations dBCD

Geometric conditions:

valid

Strength condition for linked modules (Connection activated:

No):



Float-3

ASME UHX-14 Floating Tubesheets ASME BPVC Edition 2017

Floating tubesheet according to ASME-UHX-14

Type of heat exchanger (a,b,c)	WArt	a	a,b,c
Heat Exchanger With an Immersed Floating Head			
Configuration of the tubesheet (a-f,A-D)	Type	C	a-f,A-D
Floating tubesheet gasketed, without flange extension			
Type of channel (1=Cylinder, 2=Hemispherical)			1 (1,2)
Shell side internal operation pressure	P_s	250	psi
Tube side internal operation pressure	P_t	150	psi
Shell side internal test pressure	P_{sp}		psi
Tube side internal test pressure	P_{tp}		psi
Load case (1=operation, 2+3=test at 20°C, 4=other)			1
load case: operation			
Calculation case acc. UHX-14.4(a): (1), (2) ... (7)			3 (1-7)
Tube and shell side pressure acting without thermal expansion			

Tubesheet material

Shell material (Type abc)

Tube material

Channel material(Type aefA)

Operation	Tubesheet	Shell	Tubes	Channel
Temperature	°F	°F	°F	°F
Thickness	1.75 in	in	0.083 in	0.3125 in
Outsidediameter	26.89 in	in	0.75 in	27.03 in
Poiss.-rat.	0.31	0.3	0.31	0.32
Allow. c1	0 in	in	0 in	0 in
Corr.all.c2	0 in	in	0 in	0 in

Figure

Strength for the selected load case temperature

Strength	psi	psi	psi	psi
Safety				
E-module	2.7e+7 psi	psi	2.7e+7 psi	1.48e+7 psi
Therm.dil.	1E-6/°F	1E-6/°F	1E-6/°F	4.8 1E-6/°F
Yield str.	psi	psi	20550 psi	31600 psi
Limit	°F	°F	°F	°F
temperature				
All.stress	19000 psi	0 psi	13350 psi	11300 psi
Pr.+sec.st	57000 psi	0 psi	psi	33900 psi

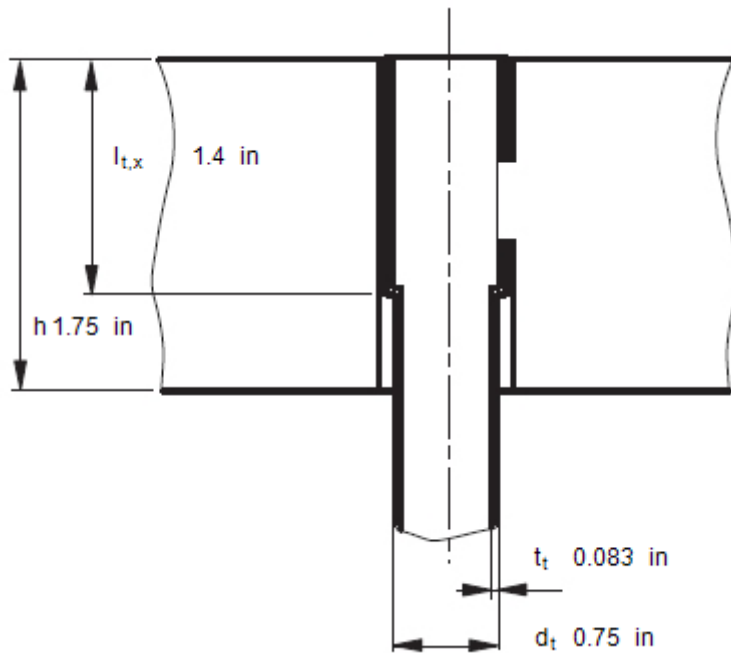
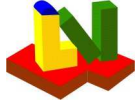
Properties for testing at 20°C

Strength	0 psi	0 psi	0 psi	0 psi
Safety				
Yield str.	psi	psi	psi	psi
Tensile str.	psi	psi	psi	psi

Additional specifications for the geometry and loading

Tubesheet

Tube-tubesheet joint	(1=expanded, 2=welded)	1 (1, 2)
Tube pattern	(1=Triangle, 2=Square)	1 (1, 2)
Number of tubes	N_t	466



Expanded length of tube in tubesheet

Expanded length ratio $l_{t,x}/h$

Radius to outermost tube hole center

Perimeter of the outermost tubes

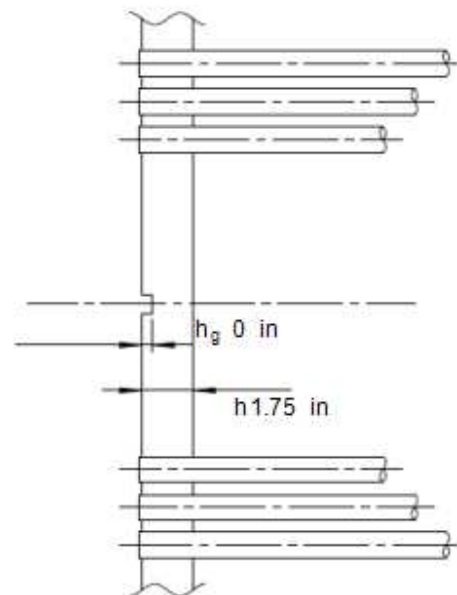
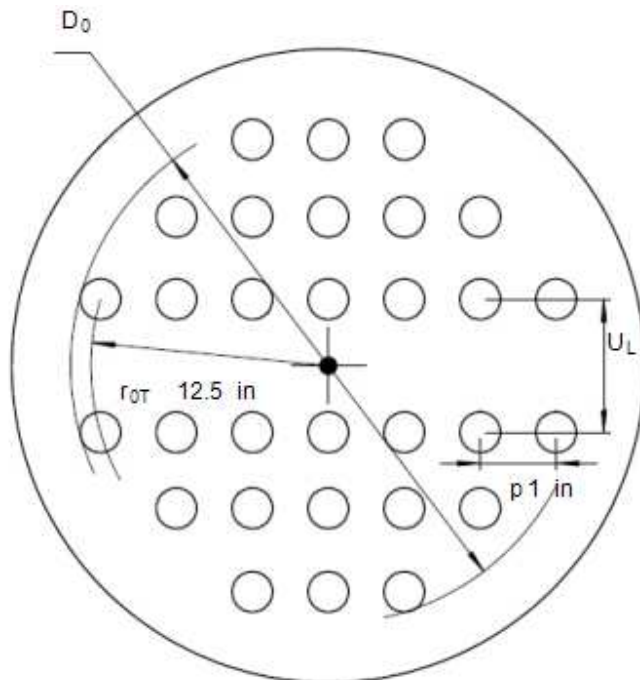
Total area enclosed by C_p

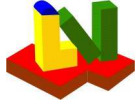
UHX-11.1(a)

UHX-12.2

UHX-12.2

$l_{t,x}$	1.4 in
ρ	0.8
r_{0T}	12.5 in
C_p	in
A_p	in ²





Tube pitch (center distance)
 Total untubed area $UL1 \cdot LL1 + UL2 \cdot LL2..$ UHX-11.2
 Depth of tube side pass partition groove
 Expanded length ratio ltx/h
 Tube length between inner tubesheet faces
 Unsupported tube span for buckling
 Type of tube support (0.6=tubesheet-tubesheet, 0.8=tubesheet - support plate, 1=plate-plate)
 Equivalent free buckling length $k \cdot l$

p 1 in
 A_L 64.4 in²
 h_g 0 in
 ρ 0.8
 L 252.5 in
 l in
 k
 l_t 15.38 in

Results acc. UHX-9

Shell

Channel

Effective seating width b in
 Gasket bolt-up force W 0 lbf
 Gasket operating force W 0 lbf
 Total required bolt area A_m 0 in²
 Flange thickness h_r 0 in

in
 lbf
 26225 lbf
 0 in²
 0 in

Maximum bolt force for all calculation cases
 Bolt root area 0 in²

W_{max} 0 lbf

: **sufficient**

Results acc. to UHX-14

Gasket seating force = $0.5(A_m + A_b) \cdot K_{sp}/S_{sp}$, App.2-5
 Channel thickness without allowances
 Shell thickness without allowances

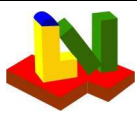
W 26225 lbf
 t_c 0.3125 in
 t_s in

Step 1 acc. UHX 14.5

Basic ligament efficiency for shear
 Effective ligament efficiency for shear
 Effective depth of pass partition groove
 Equivalent radius of outer tube limit circle
 Radial channel dimension
 Radial shell dimension
 Ratio = a_c/a_0
 Ratio = a_s/a_0
 Parameter = $1 - N_t \cdot (0.5 \cdot d_a \text{ TUBE}/a_0)^2$
 Parameter = $1 - N_t \cdot (0.5 \cdot d_i \text{ TUBE}/a_0)^2$

μ 0.25
 μ^* 0.3853
 h_g' 0 in
 a_0 12.87 in
 a_c 13.25 in
 a_s 13.25 in
 ρ_C 1.029
 ρ_S 1.029
 x_s 0.6047
 x_t 0.7603

Step 2



Step 3

Effective modulus of el. tubesheet (Fig.UHX-11.3)

Ratio of elasticity tubesheet

Effective Poisson's ratio tubesheet

Effective pitch

Effective tube hole diameter

Parameter for table UHX-13.1

Z_d 0.03276 Z_v 0.07874 Z_m 0.4213 Z_a 4.21

E^* 1.091e+7 psi

E^*/E 0.4039

ν^* 0.3084

p^* 1.068 in

d^* 0.6567 in

X_a 3.61

Z_w 0.07874

Step 4

Diameter ratio = A/D0

F 0.07417 ϕ 0.09705

K 1.044

Q_1 0.02049

UHX-14.5.5 Step 5: Coefficients

ω_C 0 in² ω_S 0 in² ω_C^* 0.07057 in²

ω_S^* 0.07057 in²

γ_b 0

Results acc. to UHX-14.6 and step 6

T_r = 68 °F T_s^* = 68 °F

P_s^* = 0 psi P_c^* = 0 psi

T_c^* 68 °F

P_e 100 psi

UHX-14.5.7 Step 7

Q_2 6.78 lbf Q_3 0.02131

Strength condition for the tubesheet bending stress, case

σ = 6330 psi $< 1.5 \cdot \sigma_B$ = 28500 psi

$< S_{PS}$ = 57000 psi

F_m 0.0751

3 :

case 1-3

case 4-7

Step 8

Strength condition for the tubesheet shear stress:

τ = 0 psi $< 0.8 \cdot \sigma_B$ = 15200 psi

Strength condition of step 7-8 are satisfied

Step 9, as examples UHX-20.3:2009 (old N)

F_q 2.925 F_s 1.787

Strength condition for the tube stress with cacluation case

S_{T0} = -1641 psi $\leq \sigma_T$ = 13350 psi

S_{T0} $\leq 2 \cdot \sigma_T$ = 26700 psi

$|S_{T0}|$ $\leq S_{tb}$ = 9188 psi

r_t 0.2376 in F_t 64.72

3 :

for calculation case 1-3

for calculation case 4-7

(for $S_{T0} < 0$, Buckling)

C_t 161

Condition UHX-14.5.9 not required for configuration ABCD

Step 10: Stress σ_S in the shell and σ_C in the channel

$\sigma_S = |\sigma_{Sm}| + |\sigma_{Sb}| = 0$ psi $< 1.5 \cdot \sigma_{allS}, S_{PSs}$ or S_{PSs1} psi

$\sigma_S = 0$ psi $|+| 0$ psi < 0 psi

$\sigma_C = |\sigma_{Cm}| + |\sigma_{Cb}| = 0$ psi $< 1.5 \cdot \sigma_{allC}$ or S_{PSc} psi

$\sigma_C = 0$ psi $|+| 0$ psi < 16950 psi

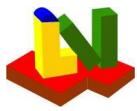
Condition UHX-14.5.10 not required for configurations dBCD

Geometric conditions:

valid

Strength condition for linked modules (Connection activated:

No):



Appendix: Material documentation

No materials for documentation