

ASME BPVC VIII-1 2019

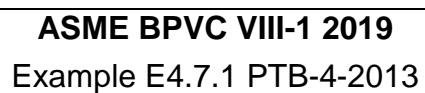
Example E4.7.1 PTB-4-2013

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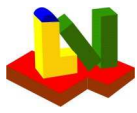
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Layout

Input values:	1.234	or	1.234
Calculated values:	1.234	or	1.234
Critical values:	1.234	or	1.234
Estimated values:	1.234	or	1.234



Strength Calculation Software		Program System ATLAS		Version		8.32.1			
Developed by Lauterbach Verfahrenstechnik GmbH									
Certified per DIN EN ISO 9001:2015		Certificate Number 01 100 044763							
				LV Soft		ASME		Diff [%]	
Example E4.7.1 - Thickness calculation for a type D Head									
	(a)	Required plate thickness t	4,25 mm	0,17 in		0,17 in		0,10%	
	Step3	Required flange thickness t	50,91 mm	2,25 in		2,25 in		0,02%	
	Step7	Total gasket seating moment Mo	11.976.492,00 N.mm	106.000,89 lbf.in		106192,50 lbf.in		0,18%	



ASME BPVC VIII-1 2019 Example E4.7.1 PTB-4-2013

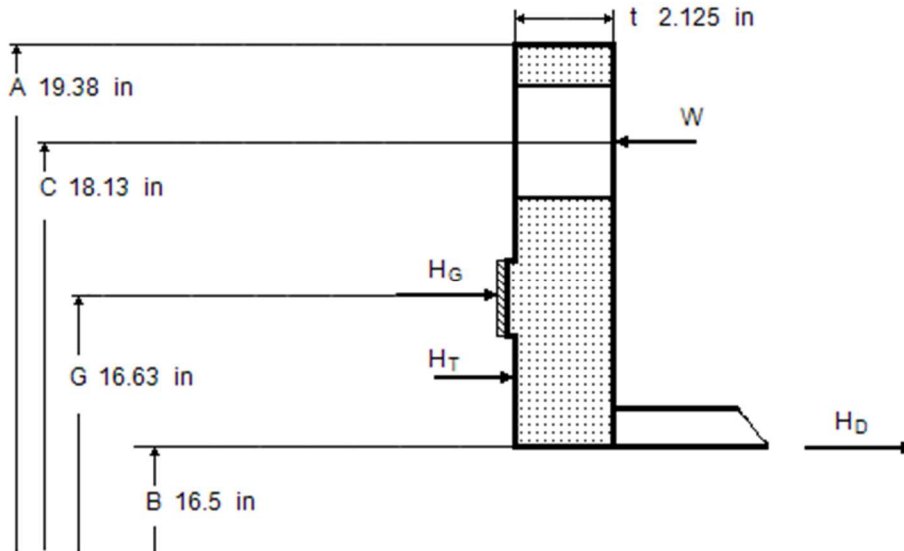
E 4.7. Step 7 - Bolted flanges - ASME BPVC VIII Division 1 App. 2: 2019

Loose Type Flange without Neck

Design data

Design pressure	P_D	213 psi	= p_D	213 psi
Hydrostatic head	D_p	0 psi	= D_p	0 psi
Calculation pressure	P_0	213 psi	= p_0	213 psi
Calculation temperature			T_0	400 °F

Flange



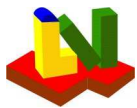
Outside diameter	A	19.38 in	Inside diameter	B	16.5 in
Bolt circle diameter	C	18.13 in	Pipe size	B_n	16.5 in
Flange thickness				t	2.125 in

Material K03504-SA-105--Class:-Size:

Cast Quality Factor	f	1
Design strength operation	S_{do}	19989 psi
Design strength installation	S_{da}	20015 psi
Allowable operating stress	S_{fb}	19989 psi
Allowable installation stress	S_{fa}	20015 psi
Corrosion allowance	c_2	0 in
Modulus of elasticity at operation	E_T	2.766e+7 psi
Modulus of elasticity at test (20°C)	E_{20}	2.92e+7 psi

Gasket

Gasket diameter	G	16.63 in
Effective gasket width	b	0.1406 in
Gasket factor	m	5.5
Gasket seating load	y	18000 psi



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Example E4.7.1 PTB-4-2013

Bolts

Number	n	20
Root diameter	d_k	0.62 in
Nominal diameter	a	0.75 in
Material	G41400-SA-193-B7-Class:-Size:<=64	
Allowable operating stress	S_b	24946 psi
Allowable installation stress	S_a	24946 psi
Consider bolt spacing correction factor B_{SC} 2-6(7)?	(N=No) Y	(Y/N)
Required operation bolt load	Eq.(1)	W_{m1} 63411 lbf
Minimum initial bolt load	Eq.(2)	W_{m2} 132116 lbf
Available cross section of bolts	A_b	6.035 in ²
Required cross section	W_{m1}/S_b	A_{m1} 2.542 in ²
Required cross section	W_{m2}/S_a	A_{m2} 5.296 in ²
Req. bolt load for gasket seating	Eq.(5) $(A_m + A_b) \cdot S_a / 2$	W 141335 lbf
Allowable bolt load	$A_b \cdot S_a$	W_{all} 150555 lbf
Design (gasket seating =1; max. allowable=2)		1 (1,2)

Moment

	Force	·	Lever arm	=	Result
$M_D = H_D \cdot h_D$	=	45522 lbf	·	0.8125 in	= 3082 lbf·ft
$M_G = H_G \cdot h_G$	=	17197 lbf	·	0.75 in	= 1075 lbf·ft
$M_T = H_T \cdot h_T$	=	692.3 lbf	·	0.7813 in	= 45.07 lbf·ft
Total operating moment	$M_{01} = F_M \cdot (M_D + M_G + M_T)$	=			4202 lbf·ft
Total gasket seating moment, Eq. (6)	$M_{02} = F_M \cdot W \cdot (C-G)/2$	=			8833 lbf·ft
Factor App.2-9 for split flange (1=full ring, 2=single split ring, 0.75=double split ring)				F_M	1 (1,2,.75)

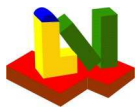
Stress

	Operation	Installation	≤ Allowable	
Longitudinal	S_H 0	0		Eq.(11)
Radial	S_R 0	0		Eq.(11)
Tangential	S_T 8234 psi	17309 psi	≤ S_f	Eq.(11)
Allowable stress	S_f 19989 psi	20015 psi		
Bolt pitch	B_S 2.847 in	≤ 3.625 in	= B_{Smax}	Eq.(3)

Remark

Cross-sectional area of bolts
Strength condition flange
Flange rigidity





Auxiliary values

$$K = \frac{A}{B} = 1.174$$

$$Y = 12.17$$

(Fig. 2-7.1)

$$H = 0.785 \cdot G^2 \cdot P \cdot 0.1 = 205571 \text{ N}$$

$$H_D = 0.785 \cdot B^2 \cdot P \cdot 0.1 = 202491 \text{ N}$$

$$H_P = 2 \cdot b \cdot \pi \cdot G \cdot m \cdot P \cdot 0.1 = 76496 \text{ N}$$

$$H_T = H - H_D = 3080 \text{ N}$$

$$W_{m1} = H + H_P = 282067 \text{ N}$$

Eq.(1)

$$W_{m2} = \pi \cdot b \cdot g \cdot y = 587676 \text{ N}$$

Eq.(2)

$$H_G = W_{m1} - H = 76496 \text{ N}$$

$$h_D = \frac{(C-B)}{2} = 20.64 \text{ mm}$$

$$h_G = \frac{(C-G)}{2} = 19.05 \text{ mm}$$

$$h_T = \frac{(h_D + h_G)}{2} = 19.84 \text{ mm}$$

Bolt pitch

$$B_S = \pi \cdot \frac{C}{n} = 72.32 \text{ mm}$$

Eq.(3)

$$B_{Smax} = 2 \cdot a + 6 \cdot \frac{t}{(m+0.5)} = 92.07 \text{ mm}$$

For

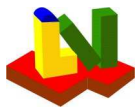
$$B_S > 2 \cdot a + t$$

Eq.(7)

$$B_{SC} = \sqrt{\frac{B_S}{(2 \cdot a + t)}} = 1$$

$$KL (=0.2 \text{ acc. Table 2-14}) = \mathbf{0.2}$$

Rigidity criterion: $J \quad \mathbf{1.289} \leq 1.0$



E 4.7.1 a - Spherically dished covers (bolted heads) - ASME VIII APPENDIX 1, 1-6 2019 Edition

Spherically dished covers as shown in Fig.: 1-6 (b)

Input

Flange moment from 2-6 or 2-11

Design pressure

Hydrostatic head

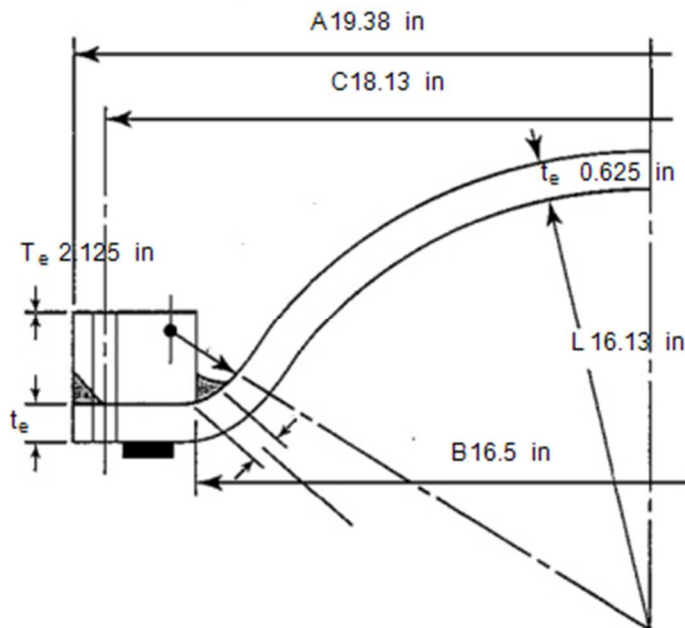
Calculation pressure

Design temperature

Gasket

M_0	8849 lbf·ft
p_D	psi
D_p	psi
p_0	213 psi
T_0	400 °F

Ring gasket



Outside diameter
Inside diameter
Bolt circle diameter
Final flange thickness

A	19.38 in
B	16.5 in
C	18.13 in
T _e	2.125 in

Crown radius
Final head thickness
Wall thickness allowance
Corrosion allowance

L	16.13 in
t _e	0.625 in
c ₁	0 in
c ₂	0.125 in

Material K02401-SA-515-60-Class:-Size:

Allowable stress

S	17114 psi
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Calculation

Required head thickness

t	0.1672 in	(1)
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Required thickness incl. allowances

t+c ₁ +c ₂	0.2922 in
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Required flange thickness (ring gasket)

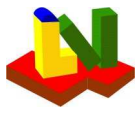
T(2)	2.166 in	(2)
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Required flange thickness (full face)

T(3)	1.224 in	(3)
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Required flange thickness

T	2.166 in	(6)
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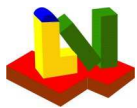
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Example E4.7.1 PTB-4-2013

Equations

$$t = \frac{5 \cdot P_0 \cdot L}{6 \cdot S} = \frac{5 \cdot 1.469 \text{ N/mm}^2 \cdot 409.6 \text{ mm}}{6 \cdot 118 \text{ N/mm}^2} = 4.248 \text{ mm} \quad (1)$$

$$T = \sqrt{\frac{|M_0|}{S \cdot B} \cdot \left[\frac{A+B}{A-B} \right]} = \sqrt{\frac{|1.2e+7 \text{ Nmm}|}{118 \text{ N/mm}^2 \cdot 419.1 \text{ mm}} \cdot \left[\frac{492.1 \text{ mm} + 419.1 \text{ mm}}{492.1 \text{ mm} - 419.1 \text{ mm}} \right]} = 55.02 \text{ mm} \quad (2)$$

$$T = 0.6 \cdot \sqrt{\frac{P}{S} \cdot \left[\frac{B \cdot (A+B) \cdot (C-B)}{A-B} \right]} = 0.6 \cdot \sqrt{\frac{1.469 \text{ N/mm}^2}{118 \text{ N/mm}^2} \cdot \left[\frac{419.1 \text{ mm} \cdot (492.1 \text{ mm} + 419.1 \text{ mm}) \cdot (460.4 \text{ mm} - 419.1 \text{ mm})}{492.1 \text{ mm} - 419.1 \text{ mm}} \right]} = 31.1 \text{ mm} \quad (3)$$



E.4.7.1 c.Step3 - Spherically dished covers (bolted heads) - ASME VIII APPENDIX 1, 1-6 2019 Edition

Spherically dished covers as shown in Fig.: 1-6 (b)

Input

Flange moment from 2-6 or 2-11

M_0 8849 lbf·ft

Design pressure

p_D psi

Hydrostatic head

D_p psi

Calculation pressure

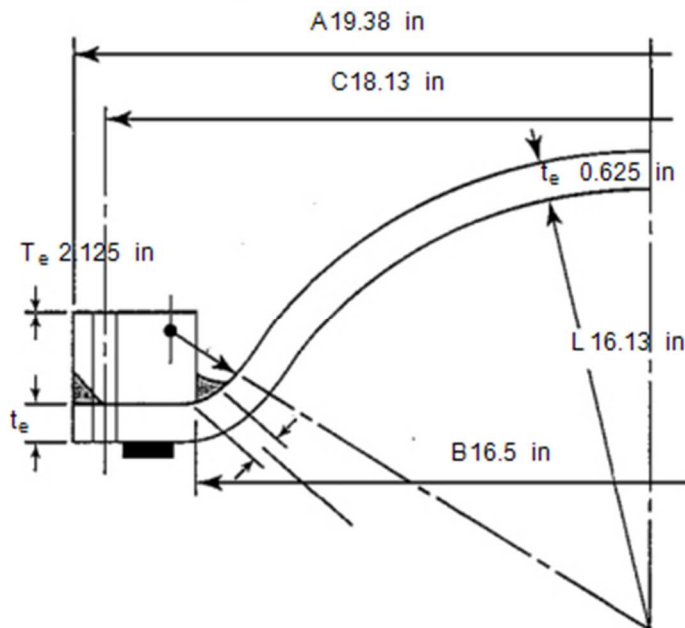
p_0 213 psi

Design temperature

T_0 400 °F

Gasket

Ring gasket



Outside diameter

A 19.38 in

Inside diameter

B 16.5 in

Bolt circle diameter

C 18.13 in

Final flange thickness

T_e 2.125 in

Crown radius

L 16.13 in

Final head thickness

t_e 0.625 in

Wall thickness allowance

c_1 0 in

Corrosion allowance

c_2 0.125 in

Material K03504-SA-105--Class:-Size:

Allowable stress

S 19989 psi

Calculation

Required head thickness

t 0.1432 in (1)

Required thickness incl. allowances

$t+c_1+c_2$ 0.2682 in

Required flange thickness (ring gasket)

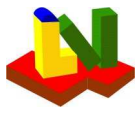
T(2) 2.004 in (2)

Required flange thickness (full face)

T(3) 1.133 in (3)

Required flange thickness

T 2.004 in (6)



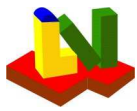
ASME BPVC VIII-1 2019
Example E4.7.1 PTB-4-2013

Equations

$$t = \frac{5 \cdot P_0 \cdot L}{6 \cdot S} = \frac{5 \cdot 1.469 \text{ N/mm}^2 \cdot 409.6 \text{ mm}}{6 \cdot 137.8 \text{ N/mm}^2} = 3.637 \text{ mm} \quad (1)$$

$$T = \sqrt{\frac{|M_0|}{S \cdot B} \cdot \left[\frac{A+B}{A-B} \right]} = \sqrt{\frac{|1.2 \text{e}+7 \text{ Nmm}|}{137.8 \text{ N/mm}^2 \cdot 419.1 \text{ mm}} \cdot \left[\frac{492.1 \text{ mm} + 419.1 \text{ mm}}{492.1 \text{ mm} - 419.1 \text{ mm}} \right]} = 50.91 \text{ mm} \quad (2)$$

$$T = 0.6 \cdot \sqrt{\frac{P}{S} \cdot \left[\frac{B \cdot (A+B) \cdot (C-B)}{A-B} \right]} = 0.6 \cdot \sqrt{\frac{1.469 \text{ N/mm}^2}{137.8 \text{ N/mm}^2} \cdot \left[\frac{419.1 \text{ mm} \cdot (492.1 \text{ mm} + 419.1 \text{ mm}) \cdot (460.4 \text{ mm} - 419.1 \text{ mm})}{492.1 \text{ mm} - 419.1 \text{ mm}} \right]} = 28.78 \text{ mm} \quad (3)$$



ASME BPVC VIII-1 2019 Example E4.7.1 PTB-4-2013

Appendix: Material documentation

Section 1: FLANSCH/E4.7.STEP7
Section 5: Tellerboden/E.4.7.1 c.Step3

Material specification:

Material code: K03504-SA-105--Class:-Size:	Regulation: ASME II.D Table 1A:2017	Spec. No.: SA-105
Short name: Carbon steel	Product: Forgings	
Delivery condition:		

Design conditions and dimensions:

Temperature [°C]: 204.44	Thickness [mm]:
Pressure [bar]: 14.69	Outside diameter [mm]:

Material values for test and design conditions:

	Test condition	Operating condition
Nominal design strength [N/mm²]:	138	137.82
Safety factor:	1	1
Allowable stress [N/mm²]:	138	137.8
Modulus of elasticity [kN/mm²]:	201.3	190.7

Notes:

G10: General Requirements

Upon prolonged exposure to temperatures above 425°C, the carbide phase of carbon steel may be converted to graphite. See Nonmandatory Appendix A, A-201 and A-202.

S1: Size Requirements

For Section I applications, stress values at temperatures of 450°C and above are permissible but, except for tubular products 75 mm O.D. or less enclosed within the boiler setting, use of these materials at these temperatures is not current practice.

T2: Time-Dependent Properties

Allowable stresses for temperatures of 400°C and above are values obtained from time-dependent properties.

Strength values at 20°C

R _{eH}	density	Tensile strength
.	.	R _m , min
N/mm²	kg/dm³	N/mm²
250	7.85	485

Strength values as a function of temperature

T	°C	40	100	150	250	325	375	425	475	525
K	N/mm²	138	138	138	136	125	117	83.9	51.1	21.3

Young's modulus-values in dependence of the temperature

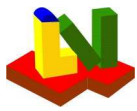
T	°C	25	100	150	200	250	300	350	400	450	500	550	600
E	kN/mm²	201	197	194	191	188	183	178	170	161	149	136	121

Mean coefficient of thermal expansion-values in dependence of the temperature

T	°C	20	100	200	300	400	500	600	700	800
α _m	1e-6/K	11.5	12.1	12.7	13.3	13.8	14.4	14.8	15.1	15.4

Differential coefficient of thermal expansion-values in dependence of the temperature

T	°C	20	100	200	300	400	500	600	700	800
α _{diff}	1e-6/K	11.5	12.7	13.8	14.9	15.9	16.7	17.0	17.1	17.7



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Example E4.7.1 PTB-4-2013

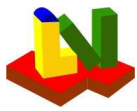
Design conditions and dimensions:

Temperature [°C]: 204.44

Thickness [mm]: 15.88

Pressure [bar]: 14.69

Outside diameter [mm]:



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Example E4.7.1 PTB-4-2013

Section 1: Schraube/E 4.7. Step 7

Material specification:

Material code: G41400-SA-193-B7-Class:-Size:<=64	Regulation: ASME II.D Table 3:2010	Spec. No.: SA-193
Short name: 1Cr-0.2Mo	Product: Bolting	
Delivery condition:		

Design conditions and dimensions:

Temperature [°C]: 204.44	Thickness [mm]:
Pressure [bar]: 14.69	Outside diameter [mm]:

Material values for test and design conditions:

	Test condition	Operating condition
Nominal design strength [N/mm²]:	172	172
Safety factor:	1	1
Allowable stress [N/mm²]:	172	172
Modulus of elasticity [kN/mm²]:	204.3	192.7

Strength values at 20°C

R _{eH}	density	Tensile strength
.	.	R _{m, min}
N/mm²	kg/dm³	N/mm²
725	7.85	860

Strength values as a function of temperature

T	°C	40	100	150	200	250	300	350	400	450	500	550
K	N/mm²	172	172	172	172	172	172	172	162	118	68.8	18.9

Young's modulus-values in dependence of the temperature

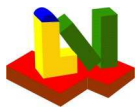
T	°C	25	100	150	200	250	300	350	400	450	500	550	600	650	700
E	kN/mm²	204	200	197	193	190	186	183	179	174	169	164	157	150	142

Mean coefficient of thermal expansion-values in dependence of the temperature

T	°C	20	100	200	300	400	500	600	700	800
α _m	1e-6/K	11.5	12.1	12.7	13.3	13.8	14.4	14.8	15.1	15.4

Differential coefficient of thermal expansion-values in dependence of the temperature

T	°C	20	100	200	300	400	500	600	700	800
α _{diff}	1e-6/K	11.5	12.7	13.8	14.9	15.9	16.7	17.0	17.1	17.7



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Example E4.7.1 PTB-4-2013

Section 3: Tellerboden/E 4.7.1 a

Material specification:

Material code: K02401-SA-515-60-Class:-Size:	Regulation: ASME II.D Table 1A:2017	Spec. No.: SA-515
Short name: Carbon steel	Product: Plate	
Delivery condition:		

Design conditions and dimensions:

Temperature [°C]: 204.44	Thickness [mm]: 15.88
Pressure [bar]: 14.69	Outside diameter [mm]:

Material values for test and design conditions:

	Test condition	Operating condition
Nominal design strength [N/mm²]:	118	118
Safety factor:	1	1
Allowable stress [N/mm²]:	118	118
Modulus of elasticity [kN/mm²]:	202.4	191.7

Notes:

G10: General Requirements

Upon prolonged exposure to temperatures above 425°C, the carbide phase of carbon steel may be converted to graphite. See Nonmandatory Appendix A, A-201 and A-202.

S1: Size Requirements

For Section I applications, stress values at temperatures of 450°C and above are permissible but, except for tubular products 75 mm O.D. or less enclosed within the boiler setting, use of these materials at these temperatures is not current practice.

T2: Time-Dependent Properties

Allowable stresses for temperatures of 400°C and above are values obtained from time-dependent properties.

Strength values at 20°C

R _{eH}	density	Tensile strength
.	.	R _{m, min}
N/mm²	kg/dm³	N/mm²
220	7.85	415

Strength values as a function of temperature

T	°C	40	100	150	250	325	375	425	475	525
K	N/mm²	118	118	118	118	112	104	75.3	45.5	21.9

Young's modulus-values in dependence of the temperature

T	°C	-200	-125	-75	25	100	150	200	250	300	350	400	450	500	550
E	kN/mm²	216	212	209	202	198	195	192	189	185	179	171	162	151	137

Mean coefficient of thermal expansion-values in dependence of the temperature

T	°C	20	100	200	300	400	500	600	700	800
α _m	1e-6/K	11.5	12.1	12.7	13.3	13.8	14.4	14.8	15.1	15.4

Differential coefficient of thermal expansion-values in dependence of the temperature

T	°C	20	100	200	300	400	500	600	700	800
α _{diff}	1e-6/K	11.5	12.7	13.8	14.9	15.9	16.7	17.0	17.1	17.7