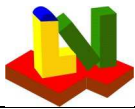
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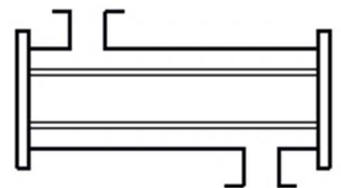
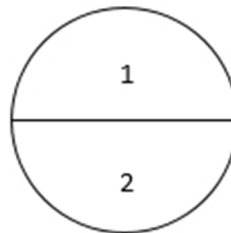
Layout

Input values:	1.234	or	1.234
Calculated values:	1.234	or	1.234
Critical values:	1.234	or	1.234
Estimated values:	1.234	or	1.234



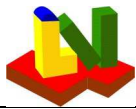
Thermal and hydraulic design of shell and tube heat exchangers

		Tube-side		Shell-side	
Medium	Water			Water	
Mass flow	$\dot{m}_i$	20 kg/s		$\dot{m}_a$	12.15 kg/s
Volume flow	$\dot{V}_i$	73.63 m³/h		$\dot{V}_a$	44.01 m³/h
Inlet pressure (abs.)	P_i	4 bar		P_a	3 bar
Inlet temperature	ϑ_{e_i}	80 °C		ϑ_{e_a}	20 °C
Outlet temperature	ϑ_{a_i}	60 °C		ϑ_{a_a}	53 °C
Mean temperature	ϑ_{m_i}	70 °C		ϑ_{m_a}	36.5 °C
Actual					
Inlet temperature	ϑ_{e_i}	80 °C		ϑ_{e_a}	20 °C
Outlet temperature	ϑ_{a_i}	59.32 °C		ϑ_{a_a}	54.12 °C
Heat duty	Q_i	-1675 kW		Q_a	1675 kW
Heat loss				Q_{v_a}	0 kW
Fouling resistance	f_i	0 m²·K/W		f_a	0 m²·K/W
Geometry					
From tubesheet library					
Installation position: Horizontal					
Bare tubes			Bare tubes		
Straight tubes with fixed tubesheets			Segmental baffles		
Shell outside diameter	D_a	406.4 mm	Shell wall thickness	s	6.3 mm
Shell inside diameter	D_i	393.8 mm	Min. bundle-to-shell clearance		12 mm
Bundle-to-shell clearance		13.18 mm			
Tube outside diameter	d_a	20 mm	Tube wall thickness	s_i	2 mm
Tube inside diameter	d_i	16 mm	Tube pitch (longitudinal)	s_2	22.52 mm
Tube pitch (transverse)	$s_{\perp}$	26 mm			
Pitch angle	Φ	60 °			
Tube lane width (horizontal)	b_h	32 mm			
Central baffle spacing		110 mm	Number of baffles / pass		24
Inlet baffle spacing		235 mm	Baffle diameter		390.8 mm
Baffle borehole diameter		20.8 mm	Baffle cut in % of shell ID		22 %
Number of sealing strips pairs		0	Baffle thickness		4 mm
Tube material			Stainless steel		
Thermal conductivity of tube material	λ		15 W/(m·K)		
Number of tube-side passes		2			
Number of shell-side passes		1			
Number of serial heat exchangers		1			



Evaluation

	Required	Final	Overdesign
Heat transfer area	A 26.57 m²	A_a 28.27 m²	6.41 %
Tube length between the tubesheets	l 2819 mm	l_a 3000 mm	



Results

Number of tubes	N	150
Heat transfer coefficient (inside)	α_i	9209 W/(m ² ·K)
Heat transfer coefficient (outside)	α_a	5784 W/(m ² ·K)
Overall heat transfer coefficient	k	2186 W/(m ² ·K)
Logarithmic mean temperature diff. LMTD	$\Delta\vartheta$	33.08 K
FN Factor (Correction factor for LMTD)	FN	0.8717
Log. mean temperature diff. (corrected) CLMTD	$\Delta\vartheta_c$	28.83 K
Total fouling resistance	f	0 m ² ·K/W

Tube-side

Velocity (tube-side)		1.356 m/s
Reynolds number	Re	52574
Pressure drop	Δp_i	16607 Pa
Mean tube wall temperature	ϑ_{w_i}	60.06 °C

Shell-side

Velocity (shell-side)		1.012 m/s
Velocity (window zone)		0.9001 m/s
Reynolds number	Re	31881
Pressure drop	Δp_a	25951 Pa
Mean tube wall temperature	ϑ_{w_a}	49.16 °C

Inlet nozzle

Nominal width	DN 125
Outside diameter	139.7 mm
Inside diameter	131.7 mm
Velocity	1.501 m/s

Inlet nozzle

Nominal width	DN 125
Outside diameter	139.7 mm
Inside diameter	131.7 mm
Velocity	0.8975 m/s
$\rho \cdot v^2$	800.3 kg/(m·s ²)

Outlet nozzle

Nominal width	DN 125
Outside diameter	139.7 mm
Inside diameter	131.7 mm
Velocity	1.501 m/s

Outlet nozzle

Nominal width	DN 125
Outside diameter	139.7 mm
Inside diameter	131.7 mm
Velocity	0.8975 m/s

Physical properties

	Tube-side
Density	ρ_i 977.9 kg/m ³
Specific heat capacity	c_{p_i} 4187 J/(kg·K)
Thermal conductivity	λ_i 0.6598 W/(m·K)
Dynamic viscosity	η_i 0.4036 mPa·s

	Shell-side
Density	ρ_a 993.6 kg/m ³
Specific heat capacity	c_{p_a} 4178 J/(kg·K)
Thermal conductivity	λ_a 0.6242 W/(m·K)
Dynamic viscosity	η_a 0.6981 mPa·s

Equations

Heat balance

$$Q_i = m_i \cdot c_{p_i} \cdot (\vartheta_{a_i} - \vartheta_{e_i}) = 20 \text{ kg/s} \cdot 4187 \text{ J/(kg·K)} \cdot (60^\circ\text{C} - 80^\circ\text{C}) = -1674976 \text{ W}$$

$$Q_a = m_a \cdot c_{p_a} \cdot (\vartheta_{a_a} - \vartheta_{e_a}) = 12.15 \text{ kg/s} \cdot 4178 \text{ J/(kg·K)} \cdot (53^\circ\text{C} - 20^\circ\text{C}) = 1674976 \text{ W}$$

$$Q_i = -(Q_a - Q_{v_a}) = -(1674976 \text{ W} - 0 \text{ W}) = -1674976 \text{ W}$$

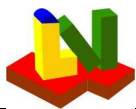
Overall heat transfer coefficient

$$\frac{1}{k} = \left[\frac{1}{\alpha_i} + f_i \right] \cdot \frac{d_a}{d_i} + \frac{d_a \cdot \ln\left(\frac{d_a}{d_i}\right)}{2 \cdot \lambda} + \frac{1}{\alpha_a} + f_a \Leftrightarrow$$

$$\frac{1}{2186 \text{ W/(m}^2\text{·K)}} = \left[\frac{1}{9209 \text{ W/(m}^2\text{·K)}} + 0 \text{ m}^2\text{·K/W} \right] \cdot \frac{0.02 \text{ m}}{0.016 \text{ m}} + \frac{0.02 \text{ m} \cdot \ln\left(\frac{0.02 \text{ m}}{0.016 \text{ m}}\right)}{2 \cdot 15 \text{ W/(m·K)}} + \frac{1}{5784 \text{ W/(m}^2\text{·K)}} + 0 \text{ m}^2\text{·K/W}$$

$$k = 2186 \text{ W/(m}^2\text{·K)}$$

$$Q = k \cdot A \cdot \Delta\vartheta \cdot FN = 2186 \text{ W/(m}^2\text{·K)} \cdot 26.57 \text{ m}^2 \cdot 33.08 \text{ K} \cdot 0.8717 = -1674976 \text{ W}$$



Tube sheet data

Description of type
Baffle-type

Segmental baffles

Shell outside diameter	D_o	406.4 mm
Shell inside diameter	D_i	393.8 mm
Minimum bundle-to-shell clearance	D_m	12 mm
Bundle-to-shell clearance	D	13.18 mm
Bundle diameter at cross flow zone	D_B	362 mm
Bundle diameter (cross flow zone and window zone)	D_{BE}	367.4 mm

Tube outside diameter	d_a	20 mm
Tube inside diameter	d_i	16 mm
Tube pitch (transverse)	s_1	26 mm
Tube pitch (longitudinal)	s_2	22.52 mm
Pitch angle	Φ	60 °

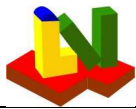
Baffle diameter	D_l	390.8 mm
Height of baffle cut	H	86.64 mm
Height of the window in % of shell inside diameter		22 %

Tube pattern staggered

Arrangement around central tube

No tubes in window?	No	
Number of tube-side passes	2	
Number of shell-side passes	1	
Tube lane width (horizontal)	32 mm	
Tube lane width (vertical)	32 mm	
Outside diameter of the head	D_a	mm
Bolt-circle diameter	D_t	mm
Number of bolts on the bolt-circle		°
Rotation angle for bolt-hole pattern		

Number of tubes	n	150
Number of dummy tubes	n_B	0
Number of tie rods	n_Z	0
Total number of tubes, dummy tubes and tie rods	n_G	150
Number of tubes, dummy tubes and tie rods in the upper and lower window	n_F	40
Number of tubes, dummy tubes and tie rods in the cross flow zone	n_S	110
Number of tube rows in a window	$n_{R,F}$	2.5
Number of tube rows in the cross flow zone	n_W	9
Number of tube rows in the end zone	$n_{W,E}$	11.5
Sum of the shortest connecting paths in the center	Le	109.8 mm
Shortest connecting path between tube and tube	e	6 mm
Shortest connecting path between tube and shell	e_1	15.91 mm
Number of connections	n_V	13
Mean distance boundary tubes - bundle centre	r_h	155.4 mm
Number of boundary tubes required/actual	RR	/ 70
Perimeter of the tube layout	C_p	1066 mm
Total area enclosed by perimeter	A_p	0.08339 m ²



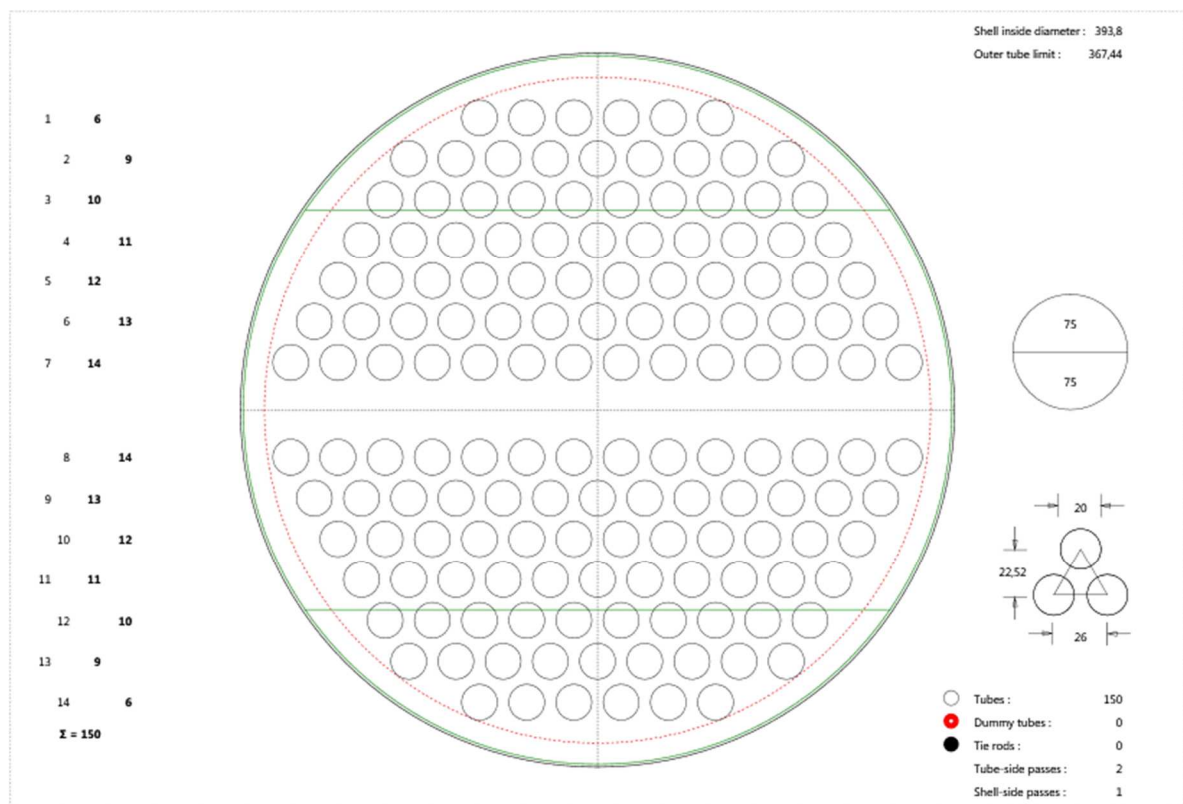
Number of tubes, dummy tubes and tie rods per pass

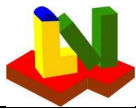
Pass-No.	1	2	3	4	5	6	7	8
	75	75	0	0	0	0	0	0

Final bundle length	l_a	3000	mm
Total area	A_{ges}	28.27	m ²
Number of baffles per shell-side path	N	24	
Central baffle spacing	S_1	110	mm
Distance between the tubesheet and the 1st baffle	S_2	235	mm
Baffle borehole diameter		20.8	mm
Number of pairs of sealing strips	n_D	0	
Number of exchangers in series		1	

Nozzles

	Tube-side	Shell-side
Inside nozzle diameter (inlet)	131.7 mm	131.7 mm
Inside nozzle diameter (outlet)	131.7 mm	131.7 mm





Properties of Water and Steam

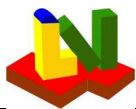
	State 1		State 2	
Calculation for saturation?	No		No	
Temperature	ϑ_1	36.5 °C	ϑ_2	49.15 °C
Pressure	p_1	3 bar	p_2	3 bar

Properties of liquid water or superheated steam

	State 1		State 2	
	Liquid		Liquid	
Density	ρ	993.6 kg/m ³	ρ	988.5 kg/m ³
Spec. isob. heat capacity	c_p	4178 J/(kg·K)	c_p	4179 J/(kg·K)
Thermal conductivity	λ	0.6242 W/(m·K)	λ	0.6397 W/(m·K)
Dynamic viscosity	η	0.6981 mPa·s	η	0.5544 mPa·s
Kinematic viscosity	ν	7.026e-7 m ² /s	ν	5.608e-7 m ² /s
Prandtl number	Pr	4.673	Pr	3.622
Thermal diffusivity	α	1.503e-7 m ² /s	α	1.548e-7 m ² /s
Specific volume	v	0.001006 m ³ /kg	v	0.001012 m ³ /kg
Spec. isoc. heat capacity	c_v	4088 J/(kg·K)	c_v	4028 J/(kg·K)
Specific enthalpy	h	153177 J/kg	h	206052 J/kg
Spec. internal energy	u	152875 J/kg	u	205749 J/kg
Specific entropy	s	525.4 J/(kg·K)	s	692.7 J/(kg·K)
Compressibility factor	Z	0.002113	Z	0.00204
Surface tension	σ	70.16 mN/m	σ	68.09 mN/m
Coefficient of thermal expansion	β	3.576e-4 1/K	β	4.516e-4 1/K
Isentropic exponent	κ	7705	κ	7862
Speed of sound	w	1525 m/s	w	1545 m/s
Dielectric constant	ϵ	74.39	ϵ	70.2

Characteristics

Molar mass	M	18.02 g/mol	Validity	$0.01^\circ\text{C} \leq \vartheta \leq 800^\circ\text{C}$
Gas constant	R	461.5 J/(kg·K)		$0.00612 \text{ bar} \leq p \leq 1000 \text{ bar}$
Critical temperature	T_c	373.9 °C		$0.01^\circ\text{C} \leq \vartheta \leq 2000^\circ\text{C}$
Critical pressure	p_c	2.206e+7 Pa		$0.00612 \text{ bar} \leq p \leq 500 \text{ bar}$
Critical density	ρ_c	322 kg/m ³		



Properties of Water and Steam

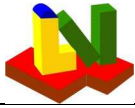
	State 1		State 2	
Calculation for saturation?	No		No	
Temperature	ϑ_1	70 °C	ϑ_2	60.06 °C
Pressure	p_1	4 bar	p_2	4 bar

Properties of liquid water or superheated steam

	State 1		State 2	
	Liquid		Liquid	
Density	ρ	977.9 kg/m ³	ρ	983.3 kg/m ³
Spec. isob. heat capacity	c_p	4187 J/(kg·K)	c_p	4182 J/(kg·K)
Thermal conductivity	λ	0.6598 W/(m·K)	λ	0.651 W/(m·K)
Dynamic viscosity	η	0.4036 mPa·s	η	0.4657 mPa·s
Kinematic viscosity	ν	4.128e-7 m ² /s	ν	4.736e-7 m ² /s
Prandtl number	Pr	2.562	Pr	2.992
Thermal diffusivity	α	1.611e-7 m ² /s	α	1.583e-7 m ² /s
Specific volume	v	0.001023 m ³ /kg	v	0.001017 m ³ /kg
Spec. isoc. heat capacity	c_v	3922 J/(kg·K)	c_v	3973 J/(kg·K)
Specific enthalpy	h	293320 J/kg	h	251707 J/kg
Spec. internal energy	u	292911 J/kg	u	251300 J/kg
Specific entropy	s	954.8 J/(kg·K)	s	831.7 J/(kg·K)
Compressibility factor	Z	0.002583	Z	0.002645
Surface tension	σ	64.48 mN/m	σ	66.23 mN/m
Coefficient of thermal expansion	β	5.838e-4 1/K	β	5.233e-4 1/K
Isentropic exponent	κ	5935	κ	5940
Speed of sound	w	1558 m/s	w	1554 m/s
Dielectric constant	ϵ	63.78	ϵ	66.77

Characteristics

Molar mass	M	18.02 g/mol	Validity	0.01°C ≤ ϑ ≤ 800°C
Gas constant	R	461.5 J/(kg·K)		0.00612 bar ≤ p ≤ 1000 bar
Critical temperature	T_c	373.9 °C		0.01°C ≤ ϑ ≤ 2000°C
Critical pressure	p_c	2.206e+7 Pa		0.00612 bar ≤ p ≤ 500 bar
Critical density	ρ_c	322 kg/m ³		



Heat transfer in pipe flow

Constant wall temperature

Process data

Total mass flow	m_{tot}	kg/h
Total volume flow	V_{tot}	m ³ /h
Number of tubes with parallel flow	Z	
Mass flow per tube	m	960 kg/h
Inlet temperature	ϑ_e	80 °C
Outlet temperature	ϑ_a	60 °C
Mean temperature	ϑ_m	70 °C
Pressure (abs.)	p	4 bar

Physical properties

Fluid liquid / gaseous?

liquid

Density	ρ	977.9 kg/m ³
Specific heat capacity	c_p	4187 J/(kg·K)
Thermal conductivity	λ	0.6598 W/(m·K)
Dynamic viscosity	η	0.4036 mPa·s
Kinematic viscosity	ν	4.128e-7 m ² /s
Prandtl number	Pr	2.562
Prandtl number at wall temperature	Pr_w	2.992
Wall temperature	ϑ_w	60.06 °C

Geometry

Tube circular / non-circular?

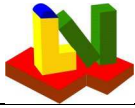
Circular tubes

Tube length	l	3000 mm
Tube inside diameter	d_i	16 mm
Cross sectional area of the tube	f	2.011e-4 m ²
Perimeter of the tube	u	50.26 mm
Hydraulic diameter	d_h	16 mm

Heat transfer

Flow velocity	w	1.356 m/s
Reynolds number	Re	52574
Nusselt number	Nu	223.3
Heat transfer coefficient	α	9209 W/(m ² ·K)

Heat duty	$Q = m_{\text{tot}} \cdot c_p \cdot (\vartheta_a - \vartheta_e)$	Q	kW
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Equations

Constant wall temperature

Turbulent flow (Re > 10000)

$$\alpha = \frac{Nu \cdot \lambda}{d_h} = \frac{223.3 \cdot 0.6598 \text{ W/(m}\cdot\text{K)}}{0.016 \text{ m}} = 9209 \text{ W/(m}^2\cdot\text{K)}$$

$$Nu = Nu_{m,T} \cdot K = 227.2 \cdot 0.9831 = 223.3$$

$$Re = \frac{w \cdot d_h \cdot \rho}{\eta} = \frac{1.356 \text{ m/s} \cdot 0.016 \text{ m} \cdot 977.9 \text{ kg/m}^3}{0.4036 \text{ mPa}\cdot\text{s}} = 52574$$

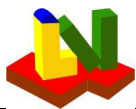
$$\xi = [1.8 \cdot \log Re - 1.5]^{-2} = [1.8 \cdot \log 52574 - 1.5]^{-2} = 0.02042$$

$$Nu_{m,T} = \frac{\frac{\xi}{8} \cdot Re \cdot Pr}{1 + 12.7 \cdot \sqrt{\frac{\xi}{8} \cdot (Pr^{2/3} - 1)}} \cdot \left[1 + \left(\frac{d_h}{l} \right)^{2/3} \right] = \frac{\frac{0.02042}{8} \cdot 52574 \cdot 2.562}{1 + 12.7 \cdot \sqrt{\frac{0.02042}{8} \cdot ((2.562)^{2/3} - 1)}} \cdot \left[1 + \left(\frac{0.016 \text{ m}}{3 \text{ m}} \right)^{2/3} \right] = 227.2$$

Correction factor K (Effect of temperature dependent property variations)

Liquids

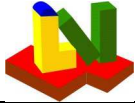
$$K = \left(\frac{Pr}{Pr_w} \right)^{0.11} = \left(\frac{2.562}{2.992} \right)^{0.11} = 0.9831$$



Heat transfer on the shell side in baffled shell and tube heat exchangers

Geometrical data

Tube arrangement	staggered	
Shell inside diameter	D_i	393.8 mm
Bundle diameter at cross flow zone	D_B	362 mm
Tube outside diameter	d_a	20 mm
Tube pitch (transverse)	s_1	26 mm
Tube pitch (longitudinal)	s_2	22.52 mm
Baffle diameter	D_l	390.8 mm
Height of baffle cut	H	86.64 mm
Diameter of the bore holes in the baffles	d_B	20.8 mm
Baffle spacing	S	110 mm
Number of tubes including blanks and support tubes	n	150
Number of tubes in the upper and lower windows	n_F	40
Number of main resistances in a cross-flow zone	n_W	9
Number of connections	n_V	13
Distance between boundary tubes and shell	e_1	15.91 mm
Shortest connecting path between tube and tube	e	6 mm
Sum of the shortest connecting paths in the center	L_E	109.8 mm
Number of sealing strip pairs	n_S	0
Number of shell-side passes	N_D	1
Fluid		
Mass flow	m	43732 kg/h
Volume flow	V	44.01 m ³ /h
Inlet temperature	ϑ_e	20 °C
Outlet temperature	ϑ_a	53 °C
Mean temperature	ϑ_m	36.5 °C
Fluid liquid /gaseous?	liquid	
Density	ρ	993.6 kg/m ³
Specific heat capacity	c_p	4178 J/(kg·K)
Thermal conductivity	λ	0.6242 W/(m·K)
Dynamic viscosity	η	0.6981 mPa·s
Kinematic viscosity	ν	7.026e-7 m ² /s
Prandtl number	Pr	4.673
Prandtl number at tube wall temperature	Pr_w	3.622
Reynolds number	$Re_{\psi,1}$	31881
Heat transfer coefficient	α	6136 W/(m ² ·K)



Results

$$\alpha = \frac{Nu_{0,AW} \cdot \lambda}{\frac{\pi}{2} \cdot d_a} \cdot K = \frac{289.8 \cdot 0.6242 \text{ W/(m}\cdot\text{K)}}{\frac{\pi}{2} \cdot 0.02 \text{ m}} \cdot 1.066 = 6136 \text{ W/(m}^2\cdot\text{K)}$$

$$Nu_{0,AW} = f_W \cdot Nu_{0,Bundle} = 0.5413 \cdot 535.3 = 289.8$$

$$f_W = f_G \cdot f_L \cdot f_B = 1.077 \cdot 0.6906 \cdot 0.728 = 0.5413$$

Calculation of $Nu_{0,Bundle}$

$$a = \frac{s_1}{d_a} = \frac{0.026 \text{ m}}{0.02 \text{ m}} = 1.3$$

$$b = \frac{s_2}{d_a} = \frac{0.02252 \text{ m}}{0.02 \text{ m}} = 1.126$$

$$\psi = 1 - \frac{\pi}{4 \cdot a} = 1 - \frac{\pi}{4 \cdot 1.3} = 0.3958$$

$$w = \frac{V}{D_i \cdot S} = \frac{0.01223 \text{ m}^3/\text{s}}{0.3938 \text{ m} \cdot 0.11 \text{ m}} = 0.2822 \text{ m/s}$$

$$Re_{\psi,1} = \frac{\frac{\pi}{2} \cdot d_a \cdot w}{\psi \cdot \nu} = \frac{\frac{\pi}{2} \cdot 0.02 \text{ m} \cdot 0.2822 \text{ m/s}}{0.3958 \cdot 7.026 \cdot 10^{-7} \text{ m}^2/\text{s}} = 31881$$

$$Nu_{1,lam} = 0.664 \cdot \sqrt{Re_{\psi,1}} \cdot \sqrt[3]{Pr} = 0.664 \cdot \sqrt{31881} \cdot \sqrt[3]{4.673} = 198.2$$

$$Nu_{1,turb} = \frac{0.037 \cdot Re_{\psi,1}^{0.8} \cdot Pr}{1 + 2.443 \cdot Re_{\psi,1}^{-0.1} \cdot (Pr^{2/3} - 1)} = \frac{0.037 \cdot (31881)^{0.8} \cdot 4.673}{1 + 2.443 \cdot (31881)^{-0.1} \cdot ((4.673)^{2/3} - 1)} = 271.2$$

$$Nu_{1,0} = 0.3 + \sqrt{Nu_{1,lam}^2 + Nu_{1,turb}^2} = 0.3 + \sqrt{(198.2)^2 + (271.2)^2} = 336.2$$

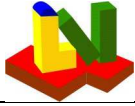
$$Nu_{0,Bundle} = f_A \cdot Nu_{1,0} = 1.592 \cdot 336.2 = 535.3$$

$$f_A = 1 + \frac{2}{3 \cdot b} = 1 + \frac{2}{3 \cdot 1.126} = 1.592$$

Calculation of f_G

$$R_G = \frac{\frac{n_F}{n}}{\left(\frac{N_D}{1}\right)} = \frac{40}{\left(\frac{150}{1}\right)} = 0.2667$$

$$f_G = 1 - R_G + 0.524 \cdot R_G^{0.32} = 1 - 0.2667 + 0.524 \cdot (0.2667)^{0.32} = 1.077$$



Calculation of f_L

$$A_{SRU} = \left(\frac{n}{N_D} - \frac{n_F}{2} \right) \cdot \frac{\pi \cdot (d_B^2 - d_a^2)}{4} = \left(\frac{150}{1} - \frac{40}{2} \right) \cdot \frac{\pi \cdot ((0.0208 \text{ m})^2 - (0.02 \text{ m})^2)}{4} = 0.003333 \text{ m}^2$$

$$\gamma = 2 \cdot \arccos \left(1 - \frac{2 \cdot H}{D_1} \right) = 2 \cdot \arccos \left(1 - \frac{2 \cdot 0.08664 \text{ m}}{0.3908 \text{ m}} \right) = 112.4^\circ$$

$$A_{SMU} = \frac{\pi}{4} \cdot (D_i^2 - D_1^2) \cdot \frac{(360 - \gamma)}{360 \cdot N_D} = \frac{\pi}{4} \cdot ((0.3938 \text{ m})^2 - (0.3908 \text{ m})^2) \cdot \frac{(360 - 112.4^\circ)}{360 \cdot 1} = 0.001272 \text{ m}^2$$

$$A_{SG} = A_{SRU} + A_{SMU} = 0.003333 \text{ m}^2 + 0.001272 \text{ m}^2 = 0.004604 \text{ m}^2$$

$$A_E = S \cdot L_E = 0.11 \text{ m} \cdot 0.1098 \text{ m} = 0.01208 \text{ m}^2$$

$$R_L = \frac{A_{SG}}{A_E} = \frac{0.004604 \text{ m}^2}{0.01208 \text{ m}^2} = 0.3811$$

$$f_L = 0.4 \cdot \frac{A_{SRU}}{A_{SG}} + \left[1 - 0.4 \cdot \frac{A_{SRU}}{A_{SG}} \right] \cdot \exp(-1.5 \cdot R_L) =$$

$$0.4 \cdot \frac{0.003333 \text{ m}^2}{0.004604 \text{ m}^2} + \left[1 - 0.4 \cdot \frac{0.003333 \text{ m}^2}{0.004604 \text{ m}^2} \right] \cdot \exp(-1.5 \cdot 0.3811) = 0.6906$$

Calculation of f_B

for $n_S \leq n_W / 2$

$$A_B = S \cdot (D_i - D_B - e) =$$

$$0.11 \text{ m} \cdot (0.3938 \text{ m} - 0.362 \text{ m} - 0.006 \text{ m}) = 0.002841 \text{ m}^2$$

for $e < (D_i - D_B)$

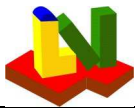
$$R_B = \frac{A_B}{A_E} = \frac{0.002841 \text{ m}^2}{0.01208 \text{ m}^2} = 0.2351$$

$$f_B = \exp \left[-\beta \cdot R_B \cdot \left(1 - \sqrt[3]{\frac{2 \cdot n_S}{n_W}} \right) \right] = \exp \left[-1.35 \cdot 0.2351 \cdot \left(1 - \sqrt[3]{\frac{2 \cdot 0}{9}} \right) \right] = 0.728$$

Correction factor K (Effect of temperature dependent property variations)

Heating of liquids

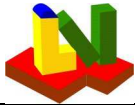
$$K = \left(\frac{Pr}{Pr_w} \right)^{0.25} = \left(\frac{4.673}{3.622} \right)^{0.25} = 1.066$$



Corrected logarithmic mean temperature difference (CLMTD) and temperature distribution according to cell method

Corrected logarithmic mean temperature difference (CLMTD) and distribution with cell method for shell and tube heat exchangers

Tube-side inlet temperature	t_{i1}	80 °C
Shell-side inlet temperature	t_{a1}	20 °C
Tube-side mass flow	m_i	72000 kg/h
Shell-side mass flow	m_a	43732 kg/h
Specific heat capacity tube-side	$c_{p,i}$	4187 J/(kg·K)
Specific heat capacity shell-side	$c_{p,a}$	4178 J/(kg·K)
Heat capacity flow tube-side; $W_{w,i} = m_i \cdot c_{p,i}$	$W_{w,i}$	83749 W/K
Heat capacity flow shell-side; $W_{w,a} = m_a \cdot c_{p,a}$	$W_{w,a}$	50757 W/K
Number of baffles	N_U	20
Number of shell-side passes	N_s	1
Number of tube-side passes	N_t	2
Sheet plus shell type		1
Number of tube rows per cell		4
Actual overall heat transfer coefficient	k	2186 W/(m²·K)
Actual heat transfer area	A	28.27 m²
0 = unmixed; 0.5 = mixed		0
Tube flow: countercurrent = 1; cocurrent = 2		1
Flow pattern: countercurrent = 1; cocurrent = 2		101
Tube-side outlet temperature	t_{i2}	59.32 °C
Shell-side outlet temperature	t_{a2}	54.12 °C
LMTD countercurrent flow	ΔT_{Geg}	32.14 K
FN factor	FN	0.8717
CLMTD corrected log. mean temperature difference	ΔT_m	28.01 K
Number of cells		42
Product $k \cdot A$		61817 W/K
Product $k \cdot A$ per cell		1472 W/K
Tube-side efficiency		0.3446
Shell-side efficiency		0.5686
Tube-side cell efficiency		0.01717
Shell-side cell efficiency		0.02834
Maximum tube-side temperature	$t_{i,max}$	80 °C
Maximum shell-side temperature	$t_{a,max}$	54.12 °C
Minimum tube-side temperature	$t_{i,min}$	59.32 °C
Minimum shell-side temperature	$t_{a,min}$	20 °C
Max. temperature inversion in one cell	t_{inv}	0 °C



Tube-side pressure drop in shell and tube heat exchangers

Physical properties

Fluid: liquid / gaseous?

Inlet temperature

Outlet temperature

Mean temperature $\vartheta_m = (\vartheta_e + \vartheta_a) / 2$

Inlet pressure (abs.)

Density

Specific heat capacity

Thermal conductivity

Dynamic viscosity

Mean temperature

liquid

ϑ_e 80 °C

ϑ_a 60 °C

ϑ_m 70 °C

P_e 4 bar

ρ 977.9 kg/m³

c_p 4187 J/(kg·K)

λ 0.6598 W/(m·K)

η 0.4036 mPa·s

Wall temperature

60.06 °C

982.6 kg/m³

0.4657 mPa·s

Geometrical data

Type: Straight tube / U-tube?

Tube outside diameter

Tube wall thickness

Tube inside diameter

Number of tube-side passes

Number of tubes per pass

Length of one tube

Inside nozzle diameter (inlet)

Inside nozzle diameter (outlet)

Acceleration due to gravity

Straight tube

d_a 20 mm

s 2 mm

d_i 16 mm

n_P 2

n_R 75

L 3000 mm

$d_{N,e}$ 131.7 mm

$d_{N,a}$ 131.7 mm

g 9.81 m/s²

Mass flow

m 20 kg/s

Volume flow

V 73.63 m³/h

Mean velocity in the tube

w 1.356 m/s

Mean velocity in the inlet nozzle

$w_{N,e}$ 1.501 m/s

Mean velocity in the outlet nozzle

$w_{N,a}$ 1.501 m/s

Reynolds number

Re 52564

Prandtl number

Pr 2.562

Grashof number

Gr 1136330

Friction factor (inlet, outlet and baffle)

Ke 3.2

Fanning friction factor (tube, isothermal)

ξ_{is} 0.006247

Correction factor for the viscosity

Φ 1.022

Correction factor for the convection

ψ 1

Friction factor (tube) ($\xi = \xi_{is} \cdot \Phi \cdot \psi$)

ξ 0.006386

Pressure drop (inlet nozzle)

$\Delta P_{N,e}$ 991.9 Pa

Pressure drop (outlet nozzle)

$\Delta P_{N,a}$ 991.9 Pa

Pressure drop (inlet, outlet and baffle)

ΔP_e 2877 Pa

Pressure drop (friction)

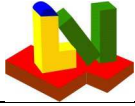
ΔP_t 8612 Pa

Fouling factor

F_t 1.364

Total pressure drop ($\Delta P = F_t \cdot \Delta P_t + \Delta P_e + \Delta P_{N,e} + \Delta P_{N,a}$)

ΔP 16607 Pa



Equations

$$w = \frac{4 \cdot m}{\pi \cdot d_i^2 \cdot n_R \cdot \rho} = \frac{4 \cdot 20 \text{ kg/s}}{\pi \cdot (0.016 \text{ m})^2 \cdot 75 \cdot 977.9 \text{ kg/m}^3} = 1.356 \text{ m/s}$$

$$w_{N,e} = \frac{4 \cdot m}{\pi \cdot d_{N,e}^2 \cdot \rho} = \frac{4 \cdot 20 \text{ kg/s}}{\pi \cdot (0.1317 \text{ m})^2 \cdot 977.9 \text{ kg/m}^3} = 1.501 \text{ m/s}$$

$$w_{N,a} = \frac{4 \cdot m}{\pi \cdot d_{N,a}^2 \cdot \rho} = \frac{4 \cdot 20 \text{ kg/s}}{\pi \cdot (0.1317 \text{ m})^2 \cdot 977.9 \text{ kg/m}^3} = 1.501 \text{ m/s}$$

$$Re = \frac{w \cdot d_i \cdot \rho}{\eta} = \frac{1.356 \text{ m/s} \cdot 0.016 \text{ m} \cdot 977.9 \text{ kg/m}^3}{4.036 \text{ e-4 Pa} \cdot \text{s}} = 52564$$

$$Pr = \eta \cdot \frac{cp}{\lambda} = 4.036 \text{ e-4 Pa} \cdot \text{s} \cdot \frac{4187 \text{ J/(kg} \cdot \text{K)}}{0.6598 \text{ W/(m} \cdot \text{K)}} = 2.562$$

$$Gr = \frac{g \cdot d_i^3 \cdot |\rho - \rho_w|}{\left(\frac{\eta}{\rho}\right)^2} = \frac{9.81 \text{ m/s}^2 \cdot (0.016 \text{ m})^3 \cdot |977.9 \text{ kg/m}^3 - 982.6 \text{ kg/m}^3|}{\left(\frac{4.036 \text{ e-4 Pa} \cdot \text{s}}{977.9 \text{ kg/m}^3}\right)^2} = 1136330$$

$$Ke = 1.6 \cdot n_P = 1.6 \cdot 2 = 3.2 \quad \text{Straight tubes, multiple passes}$$

$$\xi_{is} = 0.0035 + 0.264 \cdot Re^{-0.42} = 0.0035 + 0.264 \cdot (52564)^{-0.42} = 0.006247$$

$$\Phi = \Phi\left(Re; \eta / \eta_w\right) = \Phi(52564; 0.8667) = 1.022$$

$$\psi = \psi\left(Re; Gr \cdot Pr \cdot \eta / \eta_w\right) = \psi(52564; 2522981) = 1$$

$$\xi = \xi_{is} \cdot \Phi \cdot \psi = 0.006247 \cdot 1.022 \cdot 1 = 0.006386$$

$$\Delta P_e = Ke \cdot \rho \cdot \frac{w^2}{2} = 3.2 \cdot 977.9 \text{ kg/m}^3 \cdot \frac{(1.356 \text{ m/s})^2}{2} = 2877 \text{ Pa}$$

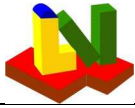
$$\Delta P_t = 2 \cdot \xi \cdot \frac{\rho \cdot w^2 \cdot n_P \cdot L}{d_i} = 2 \cdot 0.006386 \cdot \frac{977.9 \text{ kg/m}^3 \cdot (1.356 \text{ m/s})^2 \cdot 2 \cdot 3 \text{ m}}{0.016 \text{ m}} = 8612 \text{ Pa}$$

$$\Delta P_{N,e} = 0.9 \cdot \frac{\rho_e}{2} \cdot w_{N,e}^2 = 0.9 \cdot \frac{977.9 \text{ kg/m}^3}{2} \cdot (1.501 \text{ m/s})^2 = 991.9 \text{ Pa}$$

$$\Delta P_{N,a} = 0.9 \cdot \frac{\rho_a}{2} \cdot w_{N,a}^2 = 0.9 \cdot \frac{977.9 \text{ kg/m}^3}{2} \cdot (1.501 \text{ m/s})^2 = 991.9 \text{ Pa}$$

$$F_t = \left[\frac{d_a - 2 \cdot s}{d_a - 2.2 \cdot s - 0.00182 \cdot d_a^{0.3}} \right]^5 = \left[\frac{0.02 \text{ m} - 2 \cdot 0.002 \text{ m}}{0.02 \text{ m} - 2.2 \cdot 0.002 \text{ m} - 0.00182 \cdot (0.02 \text{ m})^{0.3}} \right]^5 = 1.364$$

$$\Delta P = F_t \cdot \Delta P_t + \Delta P_e + \Delta P_{N,e} + \Delta P_{N,a} = 1.364 \cdot 8612 \text{ Pa} + 2877 \text{ Pa} + 991.9 \text{ Pa} + 991.9 \text{ Pa} = 16607 \text{ Pa}$$



Tube bundle vibration analysis

General formulation

Tube outside diameter	d_a	20	mm	
Tube wall thickness	s	2	mm	
Tube inside diameter	d_i	16	mm	
Tube pitch (transverse)	s_1	26	mm	
Tube pitch (longitudinal)	s_2	22.52	mm	
Transverse pitch ratio	s_1/d_a	1.3		
Longitudinal pitch ratio	s_2/d_a	1.126		
Cross-sectional area of the tubes	A	113	mm ²	
Second moment of area of the tubes	J	4629	mm ⁴	
Modulus of elasticity	E	200000	N/mm ²	
Effective density	ρ	7850	kg/m ³	
Support for the tubes		jointed - fixed		
Factor for the support	C	3.93		
Factor for additional forces	C_f	1		
Arrangement of the tubes		Staggered bare tubes		
Strouhal number of the bundle	Sr	0.2292		
Final span	L	235	mm	345 mm
Velocity in the narrowest cross section	w_e	0.8975	m/s	1.012 m/s
Natural frequency of the tubes	f_R	1438	1/s	667.1 1/s
Safety factor	S	1.5		
Allowable excitation frequency	$f_z = f_R/S$	958.5	1/s	444.7 1/s
Excitation frequency of the flow	f_{err}	10.29	1/s	11.6 1/s

Vibration probable, if $f_{err} > f_z$

Equations

$$d_i = d_a - 2 \cdot s = 20 \text{ mm} - 2 \cdot 2 \text{ mm} = 16 \text{ mm}$$

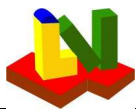
$$A = \frac{\pi}{4} \cdot [d_a^2 - d_i^2] = \frac{\pi}{4} \cdot [(20 \text{ mm})^2 - (16 \text{ mm})^2] = 113 \text{ mm}^2$$

$$J = \frac{\pi}{64} \cdot [d_a^4 - d_i^4] = \frac{\pi}{64} \cdot [(20 \text{ mm})^4 - (16 \text{ mm})^4] = 4629 \text{ mm}^4$$

$$f_R = \frac{10^6}{2 \cdot \pi} \cdot \left[\frac{C}{L} \right]^2 \cdot \sqrt{\frac{E \cdot J}{\rho \cdot A}} \cdot C_f = \frac{10^6}{2 \cdot \pi} \cdot \left[\frac{3.93}{235 \text{ mm}} \right]^2 \cdot \sqrt{\frac{200000 \text{ N/mm}^2 \cdot 4629 \text{ mm}^4}{7850 \text{ kg/m}^3 \cdot 113 \text{ mm}^2}} \cdot 1 = 1438 \text{ 1/s}$$

$$f_z = \frac{f_R}{S} = \frac{1438 \text{ 1/s}}{1.5} = 958.5 \text{ 1/s}$$

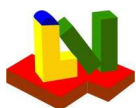
$$f_{err} = \frac{Sr \cdot w_e}{\frac{d_a}{1000}} = \frac{0.2292 \cdot 0.8975 \text{ m/s}}{\frac{20 \text{ mm}}{1000}} = 10.29 \text{ 1/s}$$



Pressure drop in the outer shell of heat exchangers

Shell-side pressure drop in shell-and-tube heat exchangers with segmental baffles

Shell inside diameter	D_i	393.8	mm
Bundle diameter at cross flow zone	D_B	362	mm
Bundle diameter (cross flow zone and window zone)	D_{BE}	367.4	mm
Tube outside diameter	d_a	20	mm
Tube pitch (transverse)	s_1	26	mm
Tube pitch (longitudinal)	s_2	22.52	mm
Pitch angle		60	°
Baffle diameter	D_l	390.8	mm
Number of baffles	n_U	24	
Height of baffle cut	H	86.64	mm
Diameter of the bore holes in the baffles	d_B	20.8	mm
Central baffle spacing	S	110	mm
Distance between the tubesheet and the 1st baffle	S_E	235	mm
Number of tubes including dummy tubes and tie rods	n	150	
Number of tubes in the upper and lower windows	n_F	40	
Number of tube rows in a window	n_{RF}	2.5	
Number of main resistances in the crossflow zone	n_W	9	
Number of main resistances in the end zone	n_{WE}	11.5	
Number of connection lines	n_V	13	
Distance between boundary tubes and shell	e_1	15.91	mm
Number of sealing strip pairs	n_S	0	
Number of shell-side passes	N_D	1	
Inside nozzle diameter (inlet)	d_{Ni}	131.7	mm
Inside nozzle diameter (outlet)	d_{No}	131.7	mm
Fluid			
Mass flow	m	43732	kg/h
Volume flow	V	44.01	m³/h
Inlet pressure	P_E	300000	Pa
Inlet temperature	ϑ_E	20	°C
Outlet temperature	ϑ_A	53	°C
Mean temperature	ϑ	36.5	°C
Fluid liquid / gaseous?		liquid	
Density	ρ	993.6	kg/m³
Specific heat capacity	c_p	4178	J/(kg·K)
Thermal conductivity	λ	0.6242	W/(m·K)
Dynamic viscosity	η	0.6981	mPa·s
Prandtl number	Pr	4.673	
Mean wall temperature	ϑ_W	49.16	°C
Dynamic viscosity at mean wall temperature	η_W	0.5544	mPa·s
Total pressure drop	Δp_{total}	25951	Pa



Shell-side pressure drop in shell-and-tube heat exchangers with segmental baffles

Cross-flow zone

$$(n_U - 1) \cdot N_D \cdot \Delta p_Q = (24 - 1) \cdot 1 \cdot 301.7 \text{ Pa} = 6939 \text{ Pa}$$

End zone

$$2 \cdot \Delta p_{Q,E} = 2 \cdot 265.9 \text{ Pa} = 531.7 \text{ Pa}$$

Window zone

$$n_U \cdot N_D \cdot \Delta p_F = 24 \cdot 1 \cdot 715.5 \text{ Pa} = 17173 \text{ Pa}$$

Shell nozzles

$$\Delta p_{N,i} + \Delta p_{N,o} = 746.8 \text{ Pa} + 560.3 \text{ Pa} = 1307 \text{ Pa}$$

Total pressure drop

$$\Delta p_{\text{total}} = 25951 \text{ Pa}$$

Results

a 1.3 b 1.126 c 1.3 e 6 mm

Cross-flow zone

L_E 109.8 mm A_E 0.01208 m² w_e 1.012 m/s

$f_{a,l,f}$ 205.1 $f_{a,t,f}$ 0.6908 $f_{a,l,v}$ 205.1

$f_{a,t,v}$ 5.342 $f_{z,l}$ 0.9896 $f_{z,t}$ 0.9682

ξ_l 0.00712 ξ_t 0.41 ξ 0.404

A_{SRU} 0.003333 m² A_{SMU} 0.001272 m² A_{SG} 0.004604 m²

R_M 0.2762 R_L 0.3811 r 0.6086

γ 112.4 ° Re 28808 β 3.7

R_S 0 R_B 0.2351 A_B 0.002841 m²

f_L 0.3892 f_B 0.4189 $\Delta p_{Q,0}$ 1850 Pa

Δp_Q 301.7 Pa

End zone

Re_E 13485 $A_{E,E}$ 0.02581 m² $w_{e,E}$ 0.4737 m/s

$f_{B,E}$ 0.4189 $\Delta p_{QE,0}$ 634.6 Pa Δp_{QE} 265.9 Pa

Window zone

A_{FG} 0.02036 m² A_{FR} 0.006283 m² A_F 0.01407 m²

w_p 0.8687 m/s w_z 0.9376 m/s n_{WF} 3.078

d_h 34.27 mm U_F 1643 mm

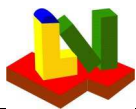
$\Delta p_{F,l}$ 884.5 Pa $\Delta p_{F,t}$ 1680 Pa Δp_F 715.5 Pa

Shell nozzles

$w_{N,i}$ 0.8975 m/s $w_{N,o}$ 0.8975 m/s

$\xi_{N,i}$ 1.866 $\xi_{N,o}$ 1.4

$\Delta p_{N,i}$ 746.8 Pa $\Delta p_{N,o}$ 560.3 Pa Δp_N 1307 Pa



CAD program for shell and tube heat exchangers

TEMA type AEL

TEMA Front head A Shell E Rear head L

	Tube-side	Shell-side
Medium	Water	Water
Inlet pressure (abs.)	p_i 400000 Pa	p_a 300000 Pa
Pressure stage	PN 5	PN 5
Inlet temperature	$\vartheta_{e,i}$ 80 °C	$\vartheta_{e,a}$ 20 °C
Outlet temperature	$\vartheta_{a,i}$ 60 °C	$\vartheta_{a,a}$ 53 °C
Mean temperature	$\vartheta_{m,i}$ 70 °C	$\vartheta_{m,a}$ 36.5 °C
Design temperature	100 °C	70 °C
Design pressure	500000 Pa	400000 Pa

Inlet nozzle	Set-on	Set-on
Type of flange	Integral flange (welding-neck) with hub	Integral flange (welding-neck) with hub
Flange connection nominal width	DN 125	DN 125
Outside diameter	139.7 mm	139.7 mm
Nozzle wall thickness	4 mm	4 mm
Inside diameter	131.7 mm	131.7 mm

Outlet nozzle	Set-on	Set-on
Type of flange	Integral flange (welding-neck) with hub	Integral flange (welding-neck) with hub
Flange connection nominal width	DN 125	DN 125
Outside diameter	139.7 mm	139.7 mm
Nozzle wall thickness	4 mm	4 mm
Inside diameter	131.7 mm	131.7 mm

CAD Data

Diameter of bore in tube sheet mm

CAD Tubesheet Configuration

Front head a - tubesheet integral with shell and channel
Rear head b - tubesheet extended as flange / integral with shell / gasketed with channel / narrow-face gasket

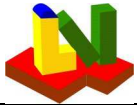
Geometry

Shell outside diameter	D_a 406.4 mm	Shell wall thickness	s_a 6.3 mm
Shell inside diameter	D_i 393.8 mm		
Bundle-shell distance	13.18 mm		
Tube outside diameter	d_a 20 mm	Tube inside diameter	d_i 16 mm
Tube pitch (transverse)	s_1 26 mm	Tube pitch (longitudinal)	s_2 22.52 mm
Pitch angle	Φ 60 °	Pass lane width	b 32 mm
Central baffle spacing	110 mm	Number of baffles/pass	24
Inlet baffle spacing	235 mm	Baffle diameter	390.8 mm
Baffle borehole diameter	20.8 mm	Baffle cut	22 %
Sealing strips pairs	0		

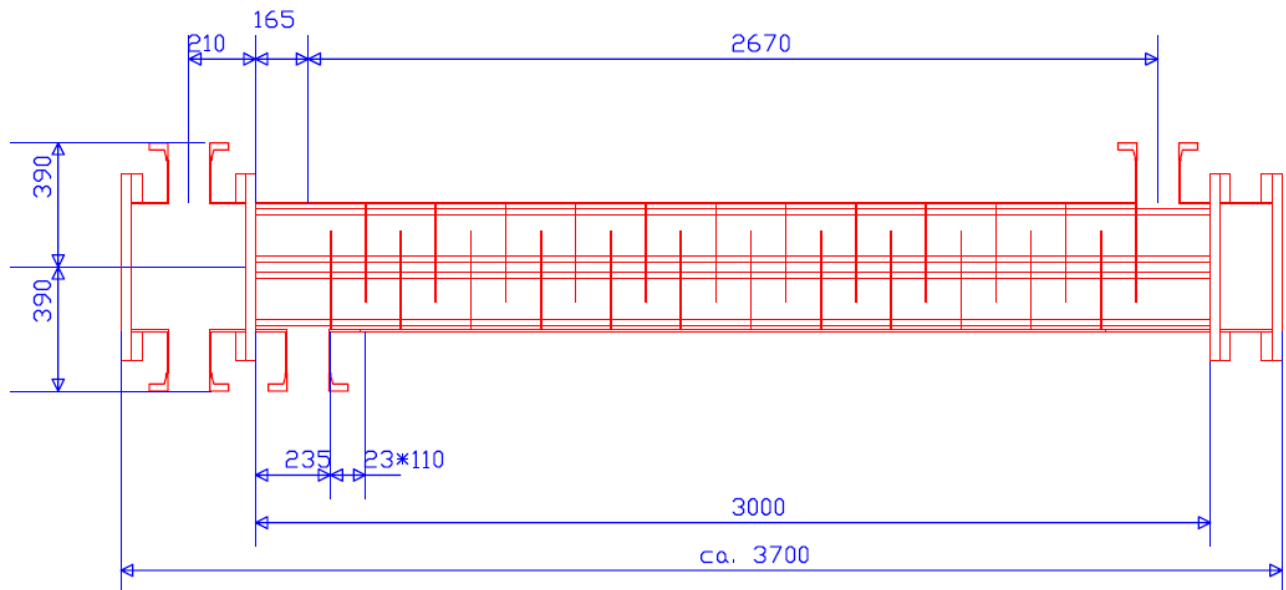
Number of tube-side passes n_t 2
Number of shell-side passes n_s 1

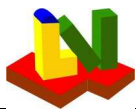
Final bundle length l_a 3000 mm
Final shell length l_a 3000 mm

Number of tubes R 150
Expansion joint diameter mm
Plate thickness (fixed plate) 30 mm
Outside diameter of tube sheet 370 mm
Plate thickness (free plate) 30 mm
Outside diameter of tube sheet (floating head) 370 mm



CAD sketch from WCAD





MS Excel specification sheet

Customer		Job No.	
Address		Reference No.	
Plant Location		Proposal No.	
TEMA-Type: AEL		Date 20.11.2017	
Installation position: Horizontal		Connected in 1 series parallel	
PERFORMANCE OF ONE UNIT			
Fluid Allocation		Shell-Side	
Fluid Name		Water	
Fluid Quantity, Total		12,15	
Vapour (In / Out)		kg/s	
Liquid (In / Out)		kg/s	
Fluid Volume Flow, Total		44,01	
Steam		m³/h	
Water			
Noncondensables			
Temperature (In / Out)		°C	
		20 53	
Density		kg/m³	
		993,6	
Viscosity		mPa·s	
		0,6981	
Molecular Weight, Vapour		kg/kmol	
Molecular Weight, Noncondensables		kg/kmol	
Specific Heat		J/(kg·K)	
		4178,3	
Thermal Conductivity		W/(m·K)	
		0,6242	
Latent Heat		J/kg	
Inlet Pressure (abs.)		bar	
		3	
Velocity		m/s	
		1,01	
Pressure Drop, Allow. / Calc.		Pa	
		25951	
Fouling Resistance		m²·K/W	
		0	
Heat Exchanged		kW	
		1675	
Transfer Rate, Service		W/(m²·K)	
		2186,3	
MTD (Corrected)		K (diff)	
		28,83	
Heat Transfer Area		m²	
		28,3	
CONSTRUCTION OF ONE SHELL		Sketch (Bundle/Nozzle Orientation)	
Design / Test Pressure		Pa	
Design Temperature		°C	
No. Passes per Shell		1 2	
Corrosion Allowance		mm	
Connections		DN 125 DN 125	
Size & Rating		DN 125 DN 125	
Tube Length		mm	
		3000	
Tube Dimensions (OD x Thk)		mm	
		20 x 2	
Pitch (Transverse)		mm	
		26	
Shell ID		mm	
		393,8	
Channel or Bonnet		Tube Material	
Tubesheet-Stationary		No. of Tubes	
Floating Head Cover		Pitch (Longitudinal)	
Baffles-Cross		Stainless steel	
Central Baffle Spacing		150	
Inlet Baffle Spacing		22,5	
Expansion Joint		Shell Dimensions (OD x Thk)	
$\rho \cdot v^2$ Bundle Entrance		406,4 x 6,3	
Gaskets-Shell Side		Channel Cover	
- Floating Head		Tubesheet-Floating	
Code Requirements		Impingement Protection	
Weight / Shell		Baffle Cut in % of Shell ID	
Weight / Bundle		Number of Baffles / Shell-Side Path	
		22	
		24	
		Number of Sealing Strips Pairs	
		Type	
		$\rho \cdot v^2$ Bundle Exit	
		Tube Side	
		TEMA Class	
		Filled with Water	
Remarks			